



TEST REPORT

ASTM E 119-05a

**Fire Tests of Building Construction
and Materials**

**2-HR FIRE RESISTANCE TEST OF A
NON-LOADBEARING WHEAT STRAW BALE WALL**

Project No. 3098054A

July 31, 2006
Revised: July 9, 2007

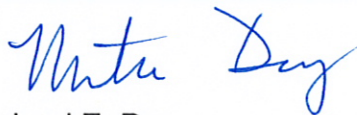
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ABSTRACT

A 10 ft x 10 ft non-loadbearing wall constructed with 7.5 pcf rectangular wheat straw bales stacked in a running bond pattern, clad on each surface with 17 GA stucco netting and 1" of cement/stucco, produced, assembled, and tested as described herein, successfully met the conditions of acceptance as outlined in ASTM Method E 119-05a Fire Tests of Building Construction and Materials for a fire endurance rating of 2 hours.

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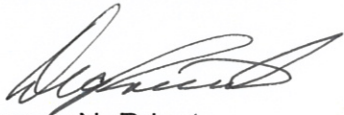


Michael E. Dey
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7/10/07

Date

Reviewed and approved:



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7/10/07

Date



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INTRODUCTION¹

"The performance of walls, columns, floors, and other building members under fire exposure conditions is an item of major importance in securing constructions that are safe, and that are not a menace to neighboring structures nor to the public. Recognition of this is registered in the codes of many authorities, municipal and other. It is important to secure balance of the many units in a single building, and of buildings of like character and use in a community; and also to promote uniformity in requirements of various authorities throughout the country. To do this it is necessary that the fire-resistive properties of materials and assemblies be measured and specified according to a common standard expressed in terms that are applicable alike to a wide variety of materials, situations, and conditions of exposure.

Such a standard is found in the methods that follow. They prescribe a standard exposing fire of controlled extent and severity. Performance is defined as the period of resistance to standard exposure elapsing before the first critical point in behavior is observed. Results are reported in units in which field exposures can be judged and expressed.

The methods may be cited as the "Standard Fire Tests," and the performance or exposure shall be expressed as "2-h," "6-h," "1/2-h," etc.

When a factor of safety exceeding that inherent in the test conditions is desired, a proportional increase should be made in the specified time-classification period.

The ASTM E 119 test procedure is identical or very similar to the following standard test methods:

UL 263
UBC 7-1
NFPA 251
ANSI A2.1
ULC S101

The analogous test standard in the International Organization of Standardization (ISO), ISO 834 Fire-resistance Tests – Elements of Building Construction, is very similar to the above U.S. test methods. Its exposure curve, as well as the method used to measure temperatures within the furnace result in a slightly less severe temperature exposure

¹ ASTM E 119-05a Standard Test Methods for Fire Tests of Building Construction and Materials ASTM International, Volume 04.07 Building Seals and Sealants, etc.

than the E 119 test for the first two hours. The ISO 834 test requires a slightly greater positive pressure within the furnace. For those reasons, the E 119 test can be considered to be slightly more severe for tests of 2 h duration or less, only if the test article is not likely to be affected by a higher furnace pressure. (BS 476 Pt 20 Fire tests on building materials and structures is virtually identical to the ISO 834 test method, as is the new CEN standard, EN 1363-1.)

1. Scope

The test methods described in this fire-test-response standard are applicable to assemblies of masonry units and to composite assemblies of structural materials for buildings, including bearing and other walls and partitions, columns, girders, beams, slabs, and composite slab and beam assemblies for floors and roofs. They are also applicable to other assemblies and structural units that constitute permanent integral parts of a finished building.

1.2 It is the intent that classifications shall register comparative performance to specific fire-test conditions during the period of exposure and shall not be construed as having determined suitability for use under other conditions or after fire exposure.

1.3 *This standard is used to measure and describe the response of materials, products, or assemblies to heat and flame under controlled conditions, but does not by itself incorporate all factors required for fire hazard or fire risk assessment of the materials, products or assemblies under actual fire conditions.*

1.4 These test methods prescribe a standard fire exposure for comparing the test results of building construction assemblies. The results of these tests are one factor in assessing predicted fire performance of building construction assemblies. Application of these test results to predict the performance of actual building construction requires the evaluation of test conditions.

1.5 The values stated in inch-pound units are to be regarded as the standard. The values given in parentheses are for information only.

1.6 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.*

1.7 The text of this standard references notes and footnotes which provide explanatory material. These notes and footnotes (excluding those in tables and figures) shall not be considered as requirements of the standard.

4. Significance and Use

4.1 This test method is intended to evaluate the duration for which the types of assemblies noted in 1.1 will contain a fire, retain their structural integrity or exhibit both properties dependent upon the type of assembly involved during a predetermined test exposure.

4.2 The test exposes a specimen to a standard fire controlled to achieve specified temperatures throughout a specified time period. When required, the fire exposure is followed by the application of a specified standard fire hose stream. The test provides a relative measure of the fire-test-response of comparable assemblies under these fire exposure conditions. The exposure is not representative of all fire conditions because conditions vary with changes in the amount, nature and distribution of fire loading, ventilation, compartment size and configuration, and heat sink characteristics of the compartment. Variation from the test conditions or specimen construction, such as size, materials, method of assembly, also affects the fire-test-response. For these reasons, evaluation of the variation is required for application to construction in the field.

4.3 The test standard provides for the following:

4.3.1 For walls, partitions and floor or roof assemblies:

4.3.1.1 Measurement of the transmission of heat.

4.3.1.2 Measurement of the transmission of hot gases through the assembly, sufficient to ignite cotton waste.

4.3.1.3 For load bearing elements, measurement of the load carrying ability of the test specimen during the test exposure.

4.3.2 For individual load bearing assemblies such as beams and columns:

4.3.2.1 Measurement of the load carrying ability under the test exposure with some consideration for the end support conditions (that is, restrained or not restrained).

4.4 The test standard does not provide the following:

4.4.1 Full information as to performance of assemblies constructed with components or lengths other than those tested.

4.4.2 Evaluation of the degree by which the assembly contributes to the fire hazard by generation of smoke, toxic gases, or other products of combustion.

4.4.3 Measurement of the degree of control or limitation of *the passage of* smoke or products of combustion through the assembly.

4.4.4 Simulation of the fire behavior of joints between building elements such as floor-wall or wall-wall, etc., connections.

4.4.5 Measurement of flame spread over surface of tested element.

4.4.6 The effect of fire endurance of conventional openings in the assembly, that is electrical receptacle outlets, plumbing pipe, etc., unless specifically provided for in the construction tested."

TEST PROCEDURE

Test Furnace

The test furnace is designed to allow the specimen to be uniformly exposed to the specified time-temperature conditions. It is fitted with 6 propane/air burners positioned on the left and right side walls, designed to allow an even heat flux distribution across the face of a test specimen while allowing no direct flame impingement. The maximum energy input into the furnace is 15 MBtu/hr. The furnace operator has controls which allow the following items to be varied during the test: the overall energy input into the furnace; the air/gas ratio to the burners; and, the input of additional air beyond that passing through the burners. The furnace opening is 14 ft wide, 12 ft tall and 4 ft deep. It may be fitted with a collar that reduces the front opening to 10 ft x 10 ft, if desired. Furnace pressures may be maintained at any value from +0.15" W.C. to -0.15" W.C. Any full-size vertical fire test furnace will have a pressure difference between the bottom and top of approximately 0.01 in. W.C. per vertical foot after operating temperatures are reached. For this reason, the furnace is operated by controlling the pressure within the furnace (with respect to the laboratory ambient pressure) by regulating the pressure at a specific horizontal plane in the furnace. The furnace pressure will often be adjusted so that the "neutral pressure plane" (that where the pressure difference between the furnace interior and the laboratory ambient is zero) is at a desired location: for instance; at the top, at a point $\frac{1}{3}$ of the way down from the top, or at the bottom of the specimen.

The temperature within the furnace is determined to be the mathematical average of thermocouples located symmetrically within the furnace and positioned six inches away from the vertical face of the test specimen. The materials used in the construction of these thermocouples are those suggested in the test standard. During the performance of a fire exposure test, the furnace temperatures are recorded every 15 seconds and displayed for the furnace operator to allow control along the specified temperature curve. For report presentation purposes, the data is saved once per minute.



This photograph of the vertical furnace shows it with a concrete adapter in place which reduces its opening to 120" x 120". Without the adapter the furnace will accept test specimens 144" tall x 168" wide. The furnace is 48" deep, with burners on the sides, so that no flame impingement on the specimen occurs.

The furnace interior temperature during a test is controlled such that the area under the time-temperature curve is within 10% of the corresponding area under the standard time-temperature curve for 1 hour or less tests, 7.5% for those less than 2 hours and 5% for those tests of 2 hours or more duration.

The fire exposure is controlled to conform with the standard time-temperature curve shown in Figure 1, as determined by the table below:

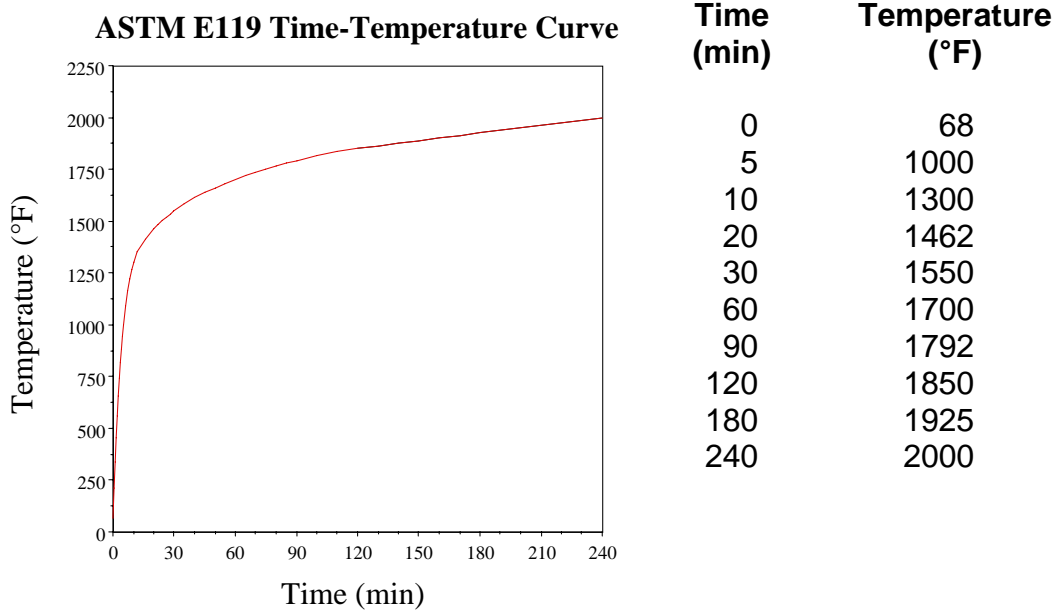


Figure 1

Fire Endurance Test

The fire exposure is continued on the specimen with its applied load if applicable, until failure occurs, or until the specimen has withstood the test conditions for the desired fire endurance rating.

Hose Stream Test

"11.1 Where required by the conditions of acceptance, the hose stream test shall be conducted to subject the specimen described in 11.2 or 11.3 to the impact, erosion, and cooling effects of a hose stream.

11.1.1 Exemption – The hose stream test shall not be required in the case of constructions having a resistance period, indicated in the fire endurance test, of less than 1 h.

11.2 The hose stream test shall be conducted on a duplicate test specimen.

11.2.1 The duplicate specimen shall be exposed to the effects of the hose stream

immediately after being subjected to a fire endurance test for a time period of one-half the fire endurance classification period determined from the fire endurance test on the initial specimen.

11.2.2 The length of time that the duplicate specimen is subjected to the fire endurance test shall not exceed 1 h.

11.3 Optional Program – As an alternative procedure, conduct the hose stream test on the initially tested specimen immediately following its fire endurance test.

11.4 In conducting the hose stream test, direct the hose stream first at the middle and then at all parts of the exposed face of the specimen. Any changes in direction shall be made slowly.

11.5 *Stream Equipment and Details* - The stream shall be delivered through a 2 1/2-in. (64-mm) hose discharging through a National Standard Playpipe of corresponding size equipped with a 1 1/8-in. (28.5-mm) discharge tip of the standard-taper smooth-bore pattern without shoulder at the orifice. The water pressure and duration of the application shall be as prescribed [in the table below]:

| Conditions For Hose Stream Test | | |
|-----------------------------------|---|---|
| Resistance Period | Water Pressure at Base of Nozzle, psi (kPa) | Duration of Application, min/100 ft ² (9 m ²) exposed area |
| 8 h and over | 45 (310) | 6 |
| 4 h and over if less than 8 h | 45 (310) | 5 |
| 2 h and over if less than 4 h | 30 (207) | 2 1/2 |
| 1-1/2 h and over if less than 2 h | 30 (207) | 1 1/2 |
| 1 h and over if less than 1-1/2 h | 30 (207) | 1 |
| Less than 1 h, if desired | 30 (207) | 1 |

11.6 *Nozzle Distance* - The distance between the tip of the nozzle and the center of the exposed surface shall be determined by the deviation from normal between the center of the nozzle axis and the center of the exposed surface of the specimen. The distance shall be 20 ft (6 m) when the axis through the center of the nozzle is normal to the center of the exposed surface. This distance shall be decreased by an amount equal to 1 ft (305 mm) for each 10° of deviation from the normal."

Correction Factor

When the indicated resistance period is $\frac{1}{2}$ h or over, determined by the average or maximum temperature rise on the unexposed surface or within the test sample, or by failure under load,, a correction shall be applied for variation of the furnace exposure from that prescribed, where it will affect the classification, by multiplying the indicated period by two thirds of the difference in area between the curve of average furnace temperature and the standard curve for the first three fourths of the period and dividing the product by the area between the standard curve and a base line of 68°F (20°C) for the same part of the indicated period, the latter area increased by 3240°F•min to compensate for the thermal lag of the furnace thermocouples during the first part of the test. For a fire exposure in the test higher than standard, the indicated resistance period shall be increased by the amount of the correction. For a fire exposure in the test lower than standard, the indicated resistance period shall be similarly decreased for fire exposure below standard. The correction is accomplished by mathematically adding the correction factor, C , to the indicated resistance period.

The correction can be expressed by the following equation:

$$C = \frac{2 I (A - A_s)}{3 (A_s + L)}$$

where:

- C = correction in the same units as I ,
- I = indicated fire-resistance period,
- A = area under the curve of indicated average furnace temperature for the first three fourths of the indicated period,
- A_s = area under the standard furnace curve for the same part of the indicated period, and
- L = lag correction in the same units as A and A_s (54°F•h or 30°C•h (3240°F•min or 1800°C•min))

CONDITIONS OF ACCEPTANCE

18. Conditions of Acceptance – [Nonloadbearing Walls]

18.1 Regard the test as successful when the following conditions are met:

18.1.1 The wall or partition has withstood the fire endurance test without passage of flame or gases hot enough to ignite cotton waste, for a period equal to that for which



classification is desired.

18.1.2 The wall or partition shall have withstood the fire and hose stream test as specified in Sections 10 and 11, without passage of flame, of gases hot enough to ignite cotton waste, or of passage of water from the hose stream. The assembly shall be considered to have failed the hose stream test if an opening develops that permits a projection of water from the stream beyond the unexposed surface during the time of the hose stream test.

18.1.3 Transmission of heat through the wall or partition during the fire endurance test shall not have been such as to raise the [average] temperature on its unexposed surface more than 250°F (139°C) above its initial temperature.

[The E 119 standard further states:]

7.4 Where the conditions of acceptance place a limitation on the rise of temperature of the unexposed surface, the temperature end point of the fire endurance period shall be determined by the average of the measurements taken at individual points; except that if a temperature rise of 30% [325°F above initial temperature] in excess of the specified limit occurs at any one of these points, the remainder shall be ignored and the fire endurance period judged as ended.

TEST SPECIMEN CONSTRUCTION

The observations and test results in this report are relevant only to the sample tested. This report by itself does not imply that the material, product, or service is or has ever been under an Intertek certification program.

The 10 ft x 10 ft wall assembly was constructed with rectangular wheat straw bales with the following nominal physical properties: 36-in long, 18-in tall (straw oriented vertically), 15-in wide, 42.3 lbs each (7.5 pcf). 2x4 lumber was fastened inside the perimeter of the test frame to act as top and bottom plates. The bales were stacked in a running bond pattern 6-1/2 courses high, completely filling the test frame. The wheat straw bales had two polypropylene ties per bale (PolyLine 430, GREENLEE®, 210 lb strength). The ties were placed in the wall in the “on-edge” orientation, meaning that the poly ties were exposed on the surface of the bales on both the heated and unheated sides. The gaps at the intersections of the stacked bales were stuffed with a mud and straw mixture that was prepared using locally available dirt plus a small amount of chopped straw mixed with enough water to hold its shape, then pushed as far into the cracks as possible. Each side of the wall was covered with 1-1/2 x 17 GA galvanized, self-furred stucco reinforcing mesh (KEYMESH®), placed underneath the bottom

course of bales and stretched vertically, with a minimum overlap of 4-in. The mesh was fastened to the 2x4s at the top of the wall using 1-1/2" long coarse thread square drive screws with 1" diameter washers, spaced nominally 6-in o.c. The stucco netting was also stapled to the 2x4s on the sides of the wall panel using 1-1/2" long galvanized fence staples spaced nominally 16" o.c. In the field, 9 GA "Robert pins" – "U" shaped wire roughly 16-in long simply bent into a "U" with 8-10" legs. The Robert pins were spaced nominally 18" o.c., and also used at overlaps and where necessary to hold the netting tighter to the bales. The bales had no interior or exterior vertical pinning. The cement / stucco was applied in two coats, each nominally 1/2" thick. The mix consisted of 1 part lime, 3 parts Portland cement, 10 parts sand, and water to a workable consistency. The stucco was applied using hand trowels.

The scratch coat was applied on June 1, 2006 by representatives of EBNet. Beginning the next morning, the stucco was wetted twice daily for four days, then covered with 6 mil thick polyethylene to hold the moisture in. The plastic was removed and the finish coat applied on June 13, 2006. The mix, application and wetting were the same for both coats of cement/stucco. Two small wooden boxes were filled with cement/stucco taken from the mix used on both days of application. These samples were sent to a local lab and compression tests were performed in accordance with ASTM C 42. Those results are located in Appendix E.

The wall was allowed to sit for 36 days prior to testing. On the morning of the test, the moisture content within the bales was measured, near each thermocouple and at three depths – exposed side, center of bale, and unexposed side. The readings were taken with a Protimeter Balemaster moisture meter. The average moisture content of 27 readings was 18.4%.

Construction drawings are located in Appendix A.

THERMOCOUPLES

All temperatures monitored on the unexposed surface of this wall assembly were measured using 24 GA., electrically-welded, Type K Chromel-Alumel, glass-glass insulated (Special Limits of Error: $\pm 1.1^{\circ}\text{C}$) thermocouples, purchased with calibration certifications and lot traceability.

To meet the requirements of ASTM E 119, nine thermocouples were installed on the unexposed surface of the wall and covered with 6 in. x 6 in. x 0.40 in. thick dry, felted, mineral fiber pads, held in place with a small daub of silicone adhesive on each corner.



These thermocouples were distributed across the unexposed surface of the wall at various locations (see Appendix B).

TEST RESULTS AND OBSERVATIONS

The test wall, contained in a non-loadbearing frame assembly, was placed in front of the Laboratory's vertical wall furnace on July 19, 2006. The thermocouple leads were then connected to the data acquisition system and their outputs verified. The laboratory air temperature was 89°F, with a relative humidity of 74%. At 11:10 a.m., the furnace was fired and the standard E 119 time-temperature curve was followed for a period of 2 hours. The pressure difference between the inside of the furnace (measured by a pressure tap located approximately 1/3 of the way down from the top of the specimen, on the horizontal centerline of the furnace) and the laboratory ambient air was maintained at -0.03 in. of water column throughout the entire test, following the first five minutes of the test, which resulted in the neutral pressure plane being positioned at the top of the test assembly.

Observations made during the test are as follows:

| Time (min:sec) | Observation |
|---------------------------|--|
| 0:00 | Start of test |
| 15:00 | Steam/smoke issuing from small cracks on the unexposed side |
| 20:00 | Popping noises coming from the exposed side, steam/smoke increasing |
| 30:00 | Small cracks have formed in the exposed stucco, with light flaming |
| 60:00 | Increase in amount of cracks and flames on the exposed side |
| 60-120:00 | No visible changes occurred |
| 120:00 | Furnace extinguished and assembly moved into position for the hose stream test |

The wall withstood the fire and hose stream tests without passage of flame, of gases hot enough to ignite cotton waste, or of the passage of water from the hose stream. No openings developed that permitted a projection of water from the stream beyond the unexposed surface during the time of the hose stream test. Transmission of heat through the wall during the fire endurance test did not raise the average temperature on the unexposed surface more than 250°F, nor any individual temperature more than 325°F.

During the fire test, the wall was measured for deflection at three points along its vertical centerline: at 30" (position #1), 60" (position #2) and 90" (position #3) from the left side of the wall. Measurements were made from a taut string to the wall surface at each location.

| <u>Time (min)</u> | <u>Position #1 (in.)</u> | <u>Position #2 (in.)</u> | <u>Position #3 (in.)</u> |
|-------------------|--------------------------|--------------------------|--------------------------|
| 0 | 1 | 2 | 7/8 |
| 20 | 1 | 2-1/4 | 1 |
| 30 | 1 | 2-1/4 | 1 |
| 55 | 1-1/8 | 2-3/8 | 1-1/8 |
| 73 | 1-1/4 | 2-1/2 | 1-1/4 |
| 100 | 1-1/4 | 2-1/2 | 1-1/4 |
| 120 | 1-1/4 | 2-1/2 | 1-1/4 |

In accordance with the E 119 test standard, a calculation for any correction to the indicated fire resistance period was done. The correction factor was then mathematically added to the indicated fire resistance period, yielding the fire resistance period achieved by this specimen:

| ITEM | DESCRIPTION | TEST VALUE |
|-------------|---|------------------------------|
| C | correction factor | -0.38 minutes -23 seconds |
| I | indicated fire-resistance period | 120 minutes |
| A | area under the curve of indicated average furnace temperature for the first three fourths of the indicated period | 132 113 (°F•min) |
| As | area under the standard furnace curve for the same part of the indicated period | 132 768 (°F•min) |
| L | lag correction | 3240 |
| | FIRE RESISTANCE PERIOD ACHIEVED BY THIS SPECIMEN ==> | 120 minutes |

Note: The standard specifies that the fire resistance be determined to the nearest integral minute. Consequently, if the correction factor is less than 30 seconds, and the test specimen met the criteria for the full indicated fire resistance period, no correction is deemed necessary. That was the case for this project.

A drawing showing the location of the thermocouples may be found in Appendix B. Listings and plots of the furnace control temperatures and specimen unexposed surface temperatures may be found in Appendix C. A photographic documentation of the test has been included in Appendix D. Results of the stucco compression testing are located in Appendix E.

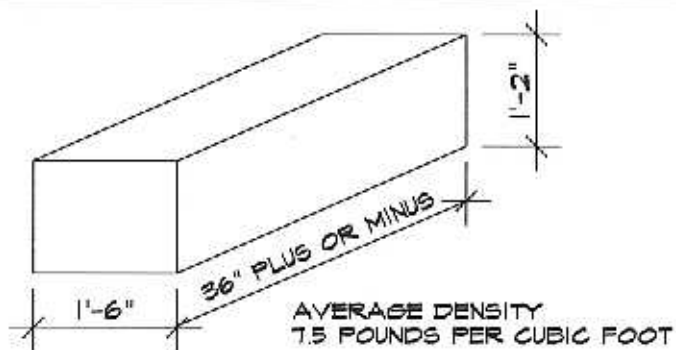
CONCLUSIONS

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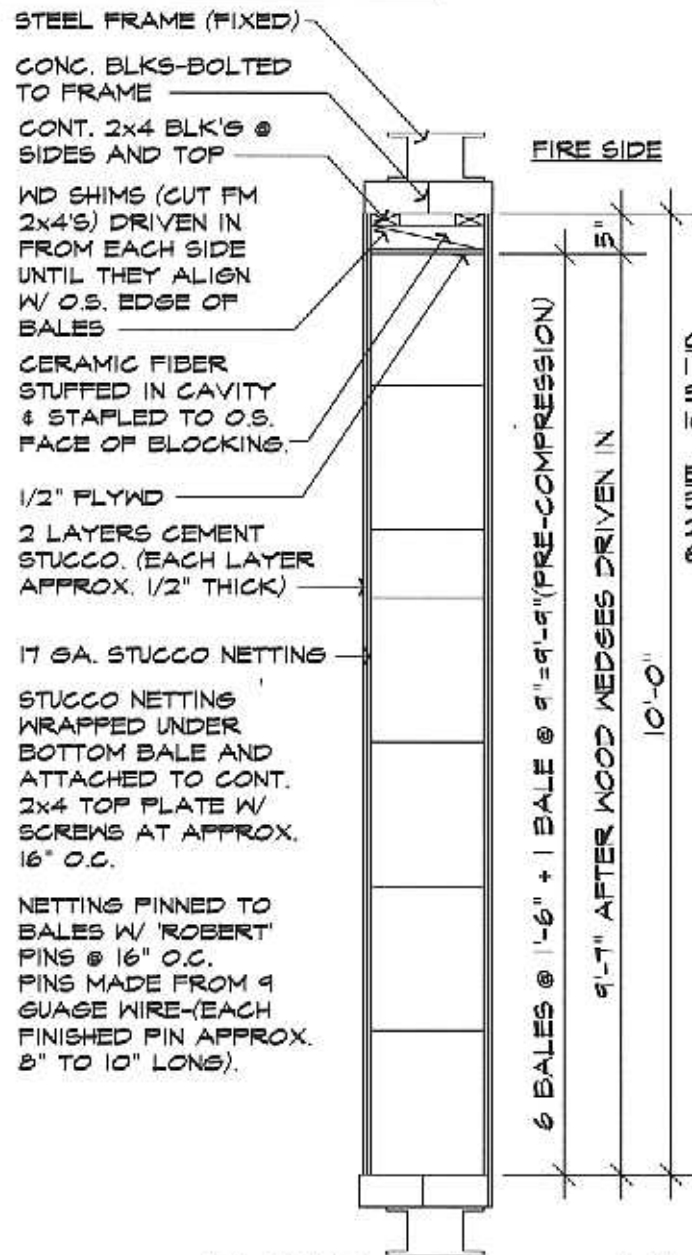
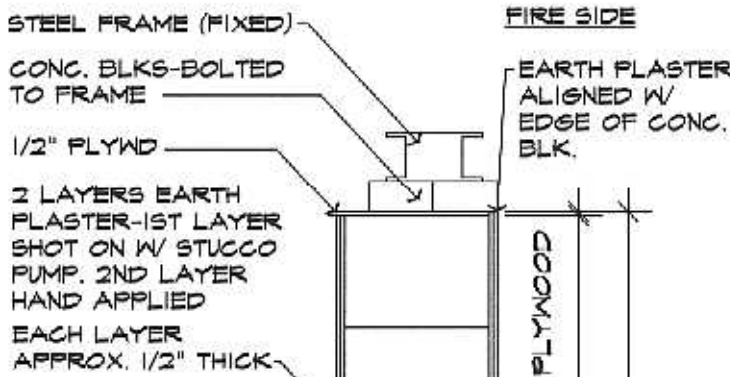
A 10 ft x 10 ft non-loadbearing wall constructed with 7.5 pcf rectangular wheat straw bales stacked in a running bond pattern, clad on each surface with 17 GA stucco netting and 1" of cement/stucco, produced, assembled, and tested as described herein, successfully met the conditions of acceptance as outlined in ASTM Method E 119-05a Fire Tests of Building Construction and Materials for a fire endurance rating of 2 hours.

APPENDIX A

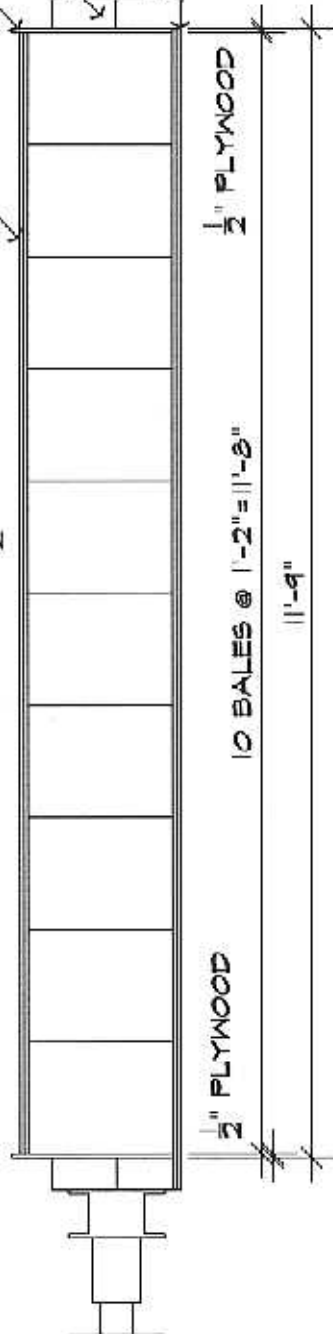
CONSTRUCTION DRAWINGS



'AVERAGE' BALE



- CEMENT STUCCO MIX:**
1 PART LIME
3 PARTS FORTLAND
10 PARTS SAND
- EARTH PLASTER MIX:**
3 PARTS CLAY
2 PARTS CHOPPED STRAW
6 PARTS SAND



CEMENT STUCCO WALL

EARTH PLASTER WALL

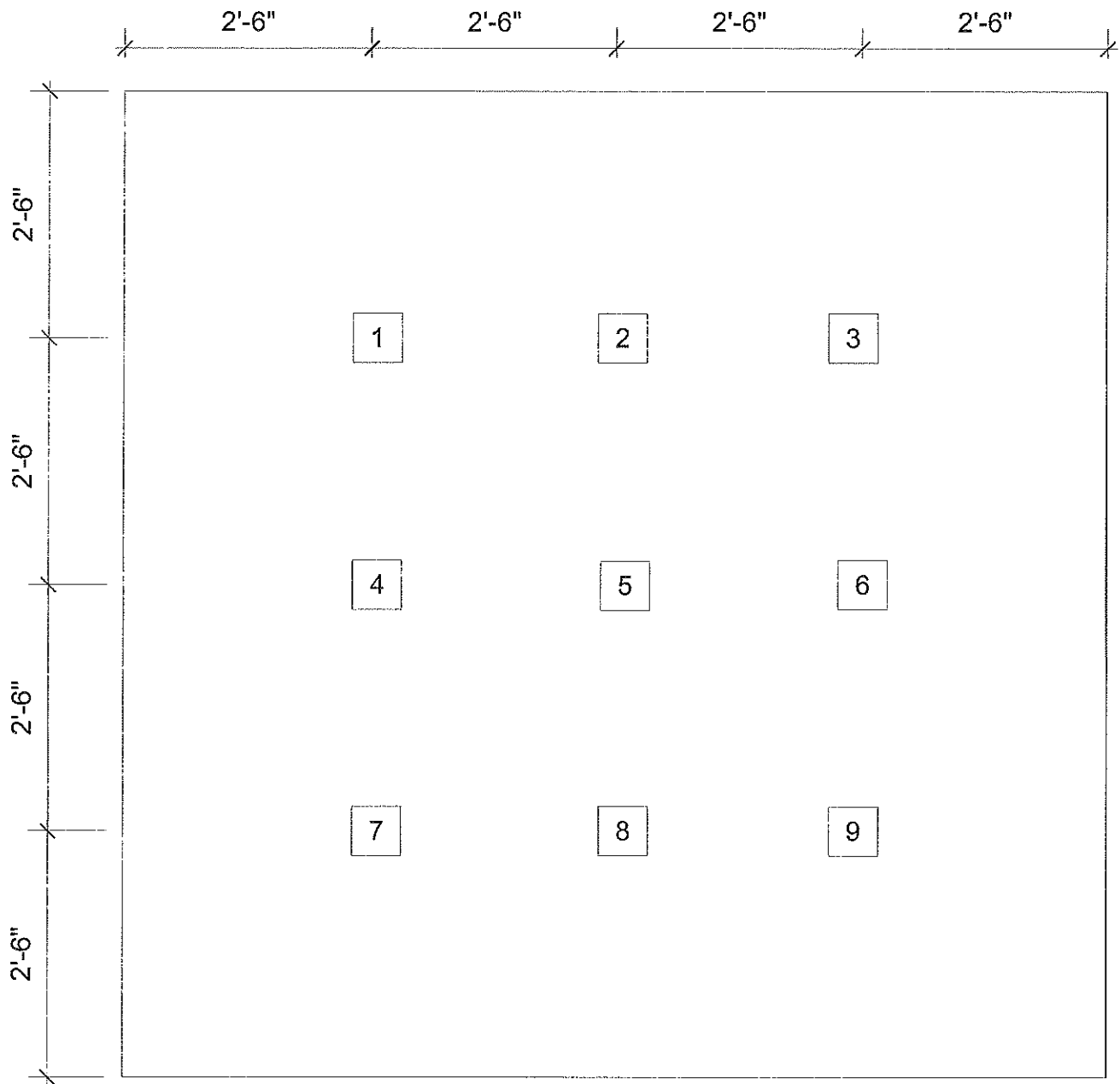
AFTER SCRATCH COAT WAS APPLIED, WALL WAS 'WETTED' DOWN ON BOTH SIDES. 6 MIL POLY WAS THEN WRAPPED OVER STRUCTURE AND TAPED TO THE FRAME TO HOLD MOISTURE IN.



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APPENDIX B

THERMOCOUPLE LAYOUT



ELEVATION VIEW

Note:

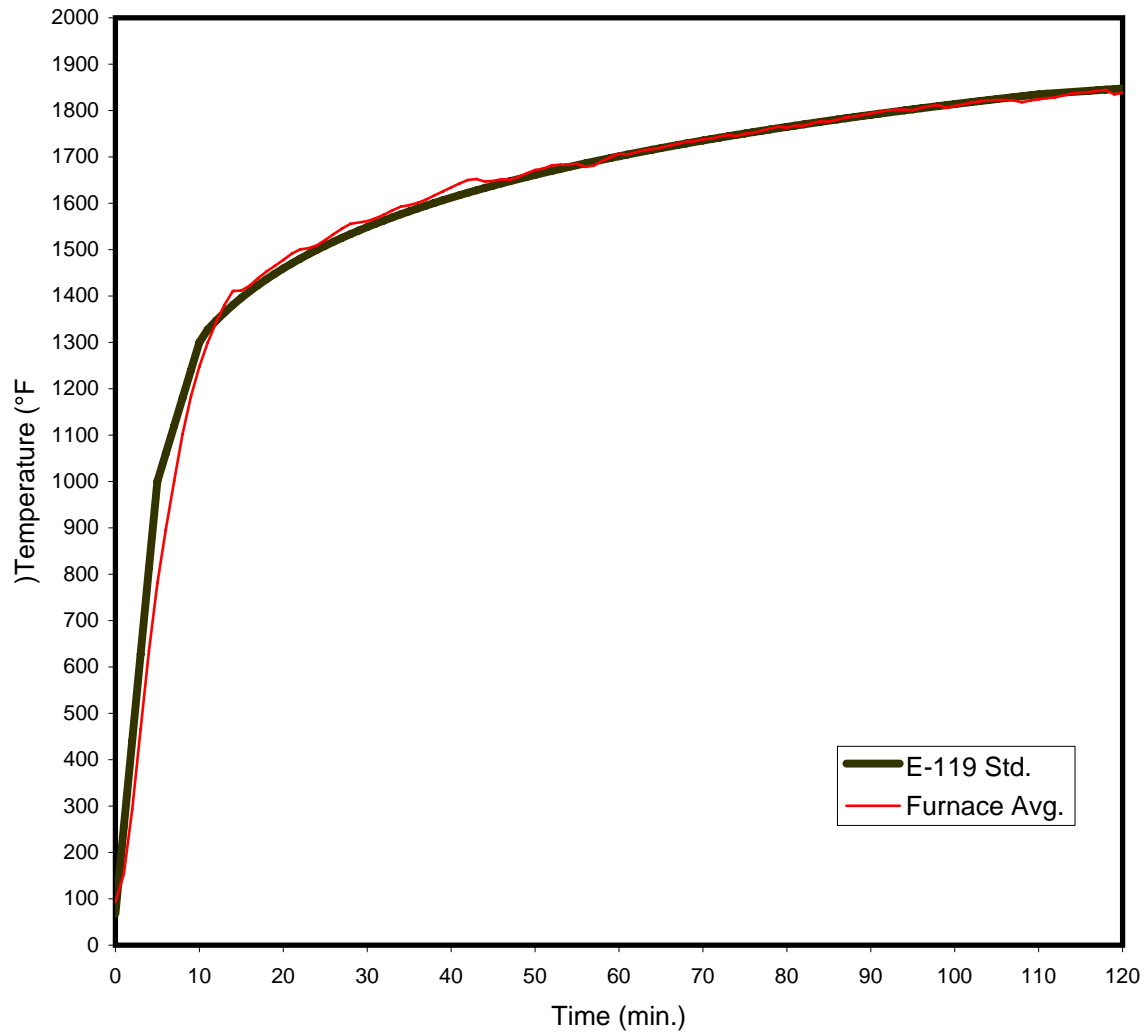
The unexposed surface was instrumented with 24 GA, fiberglass insulated Type K thermocouples as indicated in the standard, held under 6" x 6" x 0.4" thick mineral fiber pads. The TCs were located as near as possible to the locations indicated, but due to irregularities in the stucco surface, some pads were moved slightly to areas where the pad would be in full contact with the stucco surface.

| |
|--|
| Intertek Testing Services NA, Inc. Project No. 3098054A |
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| Fig. 2 Thermocouple Layout |

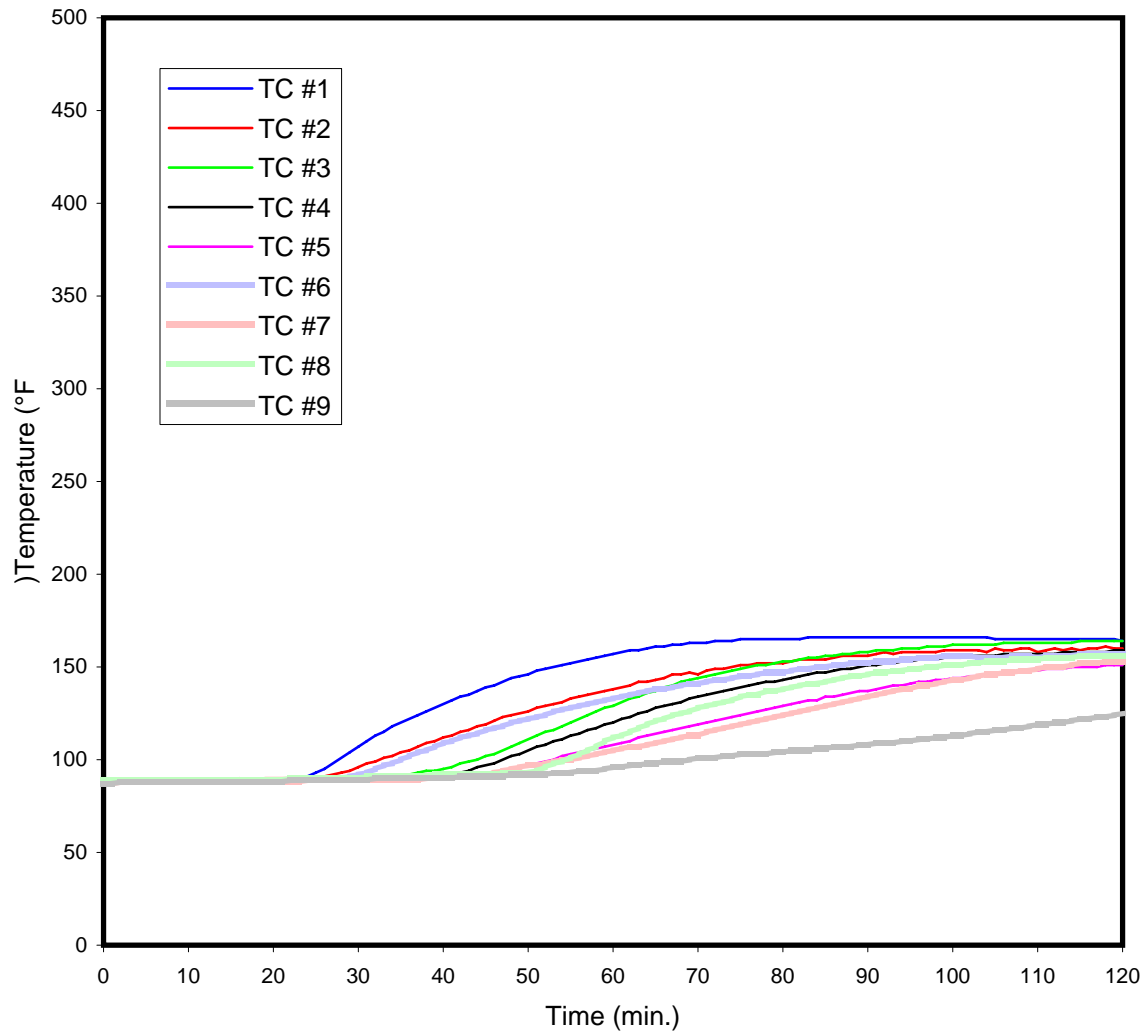
APPENDIX C

TEMPERATURE DATA

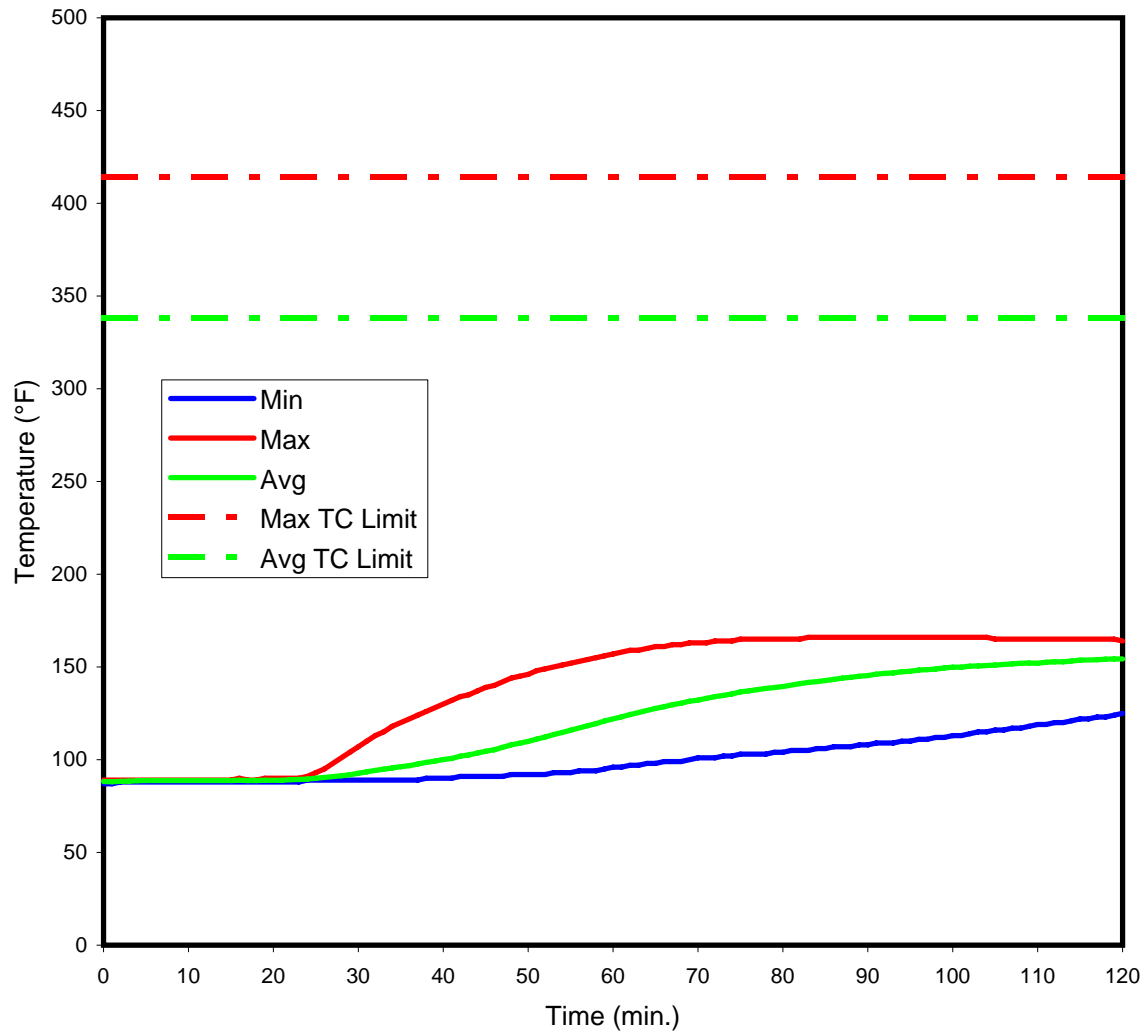
EBNet
Project No. 3098054A
Furnace Interior Temperatures



EBNet
Project No. 3098054A
Individual Cold Side Temperatures



EBNet
Project No. 3098054A
Min, Avg, Max Cold Side Temperatures



| Time (min) | E119 Std Average (°F) | Furnace Average (°F) | Integration of Furnace Average (°F•min) | Integration of E119 Std Average (°F•min) | Error (%) | Furnace Probe #1 (°F) | Furnace Probe #2 (°F) | Furnace Probe #3 (°F) |
|---------------|-----------------------------|----------------------------|--|---|--------------|--------------------------------|--------------------------------|--------------------------------|
| 0 | 68 | 92 | 0.00 | 0.00 | 0.00 | 92 | 93 | 92 |
| 1 | 254 | 153 | 54.71 | 93.20 | -41.30 | 227 | 115 | 160 |
| 2 | 441 | 293 | 209.62 | 372.80 | -43.77 | 414 | 217 | 272 |
| 3 | 627 | 465 | 520.71 | 838.80 | -37.92 | 595 | 375 | 436 |
| 4 | 814 | 635 | 1002.67 | 1491.20 | -32.76 | 748 | 537 | 593 |
| 5 | 1000 | 780 | 1641.96 | 2330.00 | -29.53 | 865 | 672 | 722 |
| 6 | 1060 | 896 | 2411.83 | 3292.00 | -26.74 | 955 | 780 | 828 |
| 7 | 1120 | 1001 | 3292.17 | 4314.00 | -23.69 | 1046 | 878 | 935 |
| 8 | 1180 | 1102 | 4275.79 | 5396.00 | -20.76 | 1137 | 977 | 1047 |
| 9 | 1240 | 1183 | 5350.62 | 6538.00 | -18.16 | 1211 | 1072 | 1130 |
| 10 | 1300 | 1248 | 6498.12 | 7740.00 | -16.04 | 1270 | 1156 | 1196 |
| 11 | 1328 | 1300 | 7703.67 | 8985.80 | -14.27 | 1317 | 1224 | 1251 |
| 12 | 1347 | 1343 | 8957.12 | 10254.99 | -12.66 | 1355 | 1281 | 1300 |
| 13 | 1364 | 1381 | 10251.29 | 11542.58 | -11.19 | 1388 | 1328 | 1340 |
| 14 | 1381 | 1411 | 11579.17 | 12847.15 | -9.87 | 1417 | 1367 | 1372 |
| 15 | 1396 | 1412 | 12922.42 | 14167.49 | -8.79 | 1418 | 1386 | 1377 |
| 16 | 1410 | 1422 | 14271.46 | 15502.53 | -7.94 | 1426 | 1398 | 1392 |
| 17 | 1424 | 1439 | 15633.92 | 16851.37 | -7.22 | 1441 | 1415 | 1412 |
| 18 | 1436 | 1453 | 17011.50 | 18213.18 | -6.60 | 1455 | 1433 | 1425 |
| 19 | 1448 | 1465 | 18402.29 | 19587.25 | -6.05 | 1466 | 1448 | 1439 |
| 20 | 1459 | 1478 | 19805.62 | 20972.92 | -5.57 | 1478 | 1462 | 1452 |
| 21 | 1470 | 1491 | 21222.12 | 22369.62 | -5.13 | 1489 | 1476 | 1467 |
| 22 | 1480 | 1500 | 22649.96 | 23776.82 | -4.74 | 1498 | 1489 | 1476 |
| 23 | 1490 | 1503 | 24083.71 | 25194.05 | -4.41 | 1502 | 1497 | 1482 |
| 24 | 1499 | 1509 | 25521.92 | 26620.85 | -4.13 | 1508 | 1502 | 1490 |
| 25 | 1508 | 1521 | 26969.00 | 28056.85 | -3.88 | 1518 | 1512 | 1500 |
| 26 | 1517 | 1533 | 28428.12 | 29501.66 | -3.64 | 1530 | 1524 | 1513 |
| 27 | 1525 | 1545 | 29899.50 | 30954.95 | -3.41 | 1540 | 1535 | 1525 |
| 28 | 1533 | 1556 | 31382.00 | 32416.40 | -3.19 | 1549 | 1546 | 1535 |
| 29 | 1541 | 1559 | 32871.12 | 33885.73 | -2.99 | 1553 | 1554 | 1539 |
| 30 | 1549 | 1562 | 34363.17 | 35362.66 | -2.83 | 1556 | 1556 | 1540 |
| 31 | 1556 | 1568 | 35859.75 | 36846.93 | -2.68 | 1560 | 1562 | 1547 |
| 32 | 1563 | 1575 | 37363.29 | 38338.32 | -2.54 | 1566 | 1569 | 1553 |
| 33 | 1570 | 1585 | 38875.33 | 39836.59 | -2.41 | 1574 | 1578 | 1563 |
| 34 | 1576 | 1593 | 40396.00 | 41341.54 | -2.29 | 1582 | 1586 | 1571 |
| 35 | 1583 | 1596 | 41922.29 | 42852.98 | -2.17 | 1585 | 1592 | 1574 |
| 36 | 1589 | 1601 | 43452.67 | 44370.71 | -2.07 | 1589 | 1597 | 1578 |
| 37 | 1595 | 1608 | 44989.00 | 45894.56 | -1.97 | 1595 | 1604 | 1584 |
| 38 | 1601 | 1617 | 46533.33 | 47424.37 | -1.88 | 1602 | 1613 | 1593 |
| 39 | 1606 | 1626 | 48086.50 | 48959.98 | -1.78 | 1610 | 1621 | 1603 |
| 40 | 1612 | 1634 | 49648.33 | 50501.24 | -1.69 | 1618 | 1629 | 1611 |
| 41 | 1617 | 1643 | 51218.79 | 52048.01 | -1.59 | 1626 | 1639 | 1620 |
| 42 | 1623 | 1650 | 52797.25 | 53600.15 | -1.50 | 1631 | 1648 | 1628 |
| 43 | 1628 | 1652 | 54380.54 | 55157.54 | -1.41 | 1632 | 1654 | 1631 |
| 44 | 1633 | 1647 | 55962.21 | 56720.06 | -1.34 | 1628 | 1654 | 1627 |
| 45 | 1638 | 1648 | 57541.75 | 58287.59 | -1.28 | 1627 | 1654 | 1629 |
| 46 | 1643 | 1652 | 59123.75 | 59860.01 | -1.23 | 1630 | 1659 | 1633 |

| Time (min) | E119 Std Average (°F) | Furnace Average (°F) | Integration of Furnace Average (°F•min) | Integration of E119 Std Average (°F•min) | Error (%) | Furnace Probe #1 (°F) | Furnace Probe #2 (°F) | Furnace Probe #3 (°F) |
|---------------|-----------------------------|----------------------------|--|---|--------------|--------------------------------|--------------------------------|--------------------------------|
| 47 | 1648 | 1651 | 60707.00 | 61437.22 | -1.19 | 1630 | 1662 | 1633 |
| 48 | 1652 | 1657 | 62292.67 | 63019.12 | -1.15 | 1635 | 1665 | 1638 |
| 49 | 1657 | 1665 | 63885.25 | 64605.62 | -1.12 | 1642 | 1673 | 1645 |
| 50 | 1661 | 1672 | 65485.37 | 66196.61 | -1.07 | 1649 | 1680 | 1652 |
| 51 | 1666 | 1675 | 67090.71 | 67792.00 | -1.03 | 1653 | 1683 | 1656 |
| 52 | 1670 | 1682 | 68701.08 | 69391.72 | -1.00 | 1658 | 1690 | 1663 |
| 53 | 1674 | 1683 | 70315.54 | 70995.68 | -0.96 | 1659 | 1693 | 1665 |
| 54 | 1678 | 1684 | 71931.00 | 72603.79 | -0.93 | 1659 | 1694 | 1666 |
| 55 | 1682 | 1685 | 73547.37 | 74215.98 | -0.90 | 1660 | 1695 | 1669 |
| 56 | 1686 | 1678 | 75161.04 | 75832.18 | -0.89 | 1658 | 1693 | 1666 |
| 57 | 1690 | 1681 | 76772.96 | 77452.32 | -0.88 | 1658 | 1690 | 1668 |
| 58 | 1694 | 1691 | 78391.33 | 79076.32 | -0.87 | 1667 | 1698 | 1678 |
| 59 | 1698 | 1700 | 80018.79 | 80704.12 | -0.85 | 1675 | 1704 | 1685 |
| 60 | 1701 | 1707 | 81653.83 | 82335.66 | -0.83 | 1681 | 1711 | 1693 |
| 61 | 1705 | 1705 | 83291.71 | 83970.87 | -0.81 | 1680 | 1712 | 1693 |
| 62 | 1709 | 1710 | 84931.42 | 85609.69 | -0.79 | 1685 | 1714 | 1698 |
| 63 | 1712 | 1715 | 86575.92 | 87252.06 | -0.77 | 1689 | 1719 | 1703 |
| 64 | 1716 | 1717 | 88223.79 | 88897.93 | -0.76 | 1692 | 1722 | 1706 |
| 65 | 1719 | 1720 | 89874.12 | 90547.25 | -0.74 | 1694 | 1724 | 1708 |
| 66 | 1722 | 1724 | 91528.08 | 92199.95 | -0.73 | 1698 | 1727 | 1712 |
| 67 | 1726 | 1729 | 93186.46 | 93856.00 | -0.71 | 1702 | 1732 | 1717 |
| 68 | 1729 | 1733 | 94849.04 | 95515.33 | -0.70 | 1706 | 1735 | 1722 |
| 69 | 1732 | 1734 | 96514.25 | 97177.91 | -0.68 | 1708 | 1737 | 1724 |
| 70 | 1735 | 1738 | 98182.08 | 98843.67 | -0.67 | 1711 | 1742 | 1728 |
| 71 | 1738 | 1740 | 99852.75 | 100512.59 | -0.66 | 1713 | 1744 | 1730 |
| 72 | 1742 | 1744 | 101526.42 | 102184.60 | -0.64 | 1716 | 1747 | 1734 |
| 73 | 1745 | 1747 | 103203.87 | 103859.68 | -0.63 | 1719 | 1750 | 1738 |
| 74 | 1748 | 1745 | 104881.96 | 105537.78 | -0.62 | 1718 | 1749 | 1737 |
| 75 | 1751 | 1750 | 106561.42 | 107218.86 | -0.61 | 1722 | 1753 | 1741 |
| 76 | 1753 | 1752 | 108244.25 | 108902.87 | -0.60 | 1725 | 1756 | 1743 |
| 77 | 1756 | 1757 | 109930.42 | 110589.78 | -0.60 | 1729 | 1759 | 1747 |
| 78 | 1759 | 1761 | 111621.33 | 112279.55 | -0.59 | 1734 | 1765 | 1752 |
| 79 | 1762 | 1765 | 113316.58 | 113972.15 | -0.58 | 1738 | 1767 | 1755 |
| 80 | 1765 | 1763 | 115012.62 | 115667.54 | -0.57 | 1737 | 1767 | 1754 |
| 81 | 1768 | 1768 | 116709.83 | 117365.68 | -0.56 | 1741 | 1771 | 1758 |
| 82 | 1770 | 1767 | 118409.04 | 119066.55 | -0.55 | 1742 | 1774 | 1759 |
| 83 | 1773 | 1773 | 120110.83 | 120770.10 | -0.55 | 1746 | 1779 | 1764 |
| 84 | 1776 | 1777 | 121817.50 | 122476.30 | -0.54 | 1750 | 1783 | 1766 |
| 85 | 1778 | 1776 | 123525.79 | 124185.13 | -0.53 | 1750 | 1783 | 1766 |
| 86 | 1781 | 1780 | 125235.87 | 125896.55 | -0.52 | 1753 | 1788 | 1771 |
| 87 | 1783 | 1785 | 126950.46 | 127610.53 | -0.52 | 1758 | 1792 | 1775 |
| 88 | 1786 | 1787 | 128668.42 | 129327.04 | -0.51 | 1760 | 1794 | 1777 |
| 89 | 1788 | 1791 | 130389.17 | 131046.06 | -0.50 | 1764 | 1798 | 1781 |
| 90 | 1791 | 1794 | 132113.33 | 132767.56 | -0.49 | 1767 | 1801 | 1784 |
| 91 | 1793 | 1797 | 133840.79 | 134491.50 | -0.48 | 1770 | 1805 | 1788 |
| 92 | 1796 | 1800 | 135571.33 | 136217.86 | -0.47 | 1773 | 1809 | 1792 |
| 93 | 1798 | 1802 | 137304.17 | 137946.62 | -0.47 | 1776 | 1811 | 1793 |

| Time (min) | E119 Std Average (°F) | Furnace Average (°F) | Integration of Furnace Average (°F•min) | Integration of E119 Std Average (°F•min) | Error (%) | Furnace Probe #1 (°F) | Furnace Probe #2 (°F) | Furnace Probe #3 (°F) |
|---------------|-----------------------------|----------------------------|--|---|--------------|--------------------------------|--------------------------------|--------------------------------|
| 94 | 1800 | 1802 | 139037.92 | 139677.75 | -0.46 | 1777 | 1813 | 1794 |
| 95 | 1803 | 1801 | 140771.25 | 141370.00 | -0.42 | 1776 | 1811 | 1794 |
| 96 | 1805 | 1806 | 142506.54 | 143105.00 | -0.42 | 1780 | 1814 | 1799 |
| 97 | 1807 | 1810 | 144246.25 | 144842.50 | -0.41 | 1784 | 1817 | 1803 |
| 98 | 1809 | 1812 | 145989.00 | 146582.50 | -0.40 | 1787 | 1821 | 1806 |
| 99 | 1812 | 1806 | 147729.83 | 148324.50 | -0.40 | 1782 | 1817 | 1801 |
| 100 | 1814 | 1810 | 149469.71 | 150068.50 | -0.40 | 1785 | 1819 | 1805 |
| 101 | 1816 | 1813 | 151213.37 | 151815.00 | -0.40 | 1789 | 1821 | 1809 |
| 102 | 1818 | 1817 | 152960.67 | 153564.00 | -0.39 | 1792 | 1824 | 1813 |
| 103 | 1820 | 1820 | 154711.21 | 155315.00 | -0.39 | 1795 | 1827 | 1816 |
| 104 | 1823 | 1822 | 156464.08 | 157068.00 | -0.38 | 1797 | 1828 | 1817 |
| 105 | 1825 | 1822 | 158218.17 | 158823.00 | -0.38 | 1798 | 1828 | 1818 |
| 106 | 1827 | 1823 | 159972.75 | 160580.00 | -0.38 | 1799 | 1830 | 1819 |
| 107 | 1829 | 1822 | 161727.17 | 162339.00 | -0.38 | 1798 | 1830 | 1818 |
| 108 | 1831 | 1818 | 163479.12 | 164100.00 | -0.38 | 1795 | 1827 | 1815 |
| 109 | 1833 | 1822 | 165230.92 | 165863.00 | -0.38 | 1798 | 1828 | 1818 |
| 110 | 1835 | 1824 | 166985.87 | 167628.00 | -0.38 | 1801 | 1830 | 1822 |
| 111 | 1836 | 1827 | 168743.37 | 169395.00 | -0.38 | 1803 | 1832 | 1825 |
| 112 | 1838 | 1829 | 170503.04 | 171163.50 | -0.39 | 1805 | 1834 | 1826 |
| 113 | 1839 | 1833 | 172265.71 | 172933.00 | -0.39 | 1810 | 1837 | 1831 |
| 114 | 1840 | 1837 | 174032.50 | 174704.00 | -0.38 | 1814 | 1842 | 1835 |
| 115 | 1841 | 1838 | 175802.04 | 176476.50 | -0.38 | 1815 | 1844 | 1836 |
| 116 | 1843 | 1840 | 177573.08 | 178250.00 | -0.38 | 1817 | 1845 | 1837 |
| 117 | 1844 | 1842 | 179346.12 | 180024.50 | -0.38 | 1820 | 1848 | 1840 |
| 118 | 1845 | 1845 | 181121.50 | 181800.50 | -0.37 | 1822 | 1850 | 1843 |
| 119 | 1846 | 1835 | 182893.12 | 183578.00 | -0.37 | 1815 | 1845 | 1834 |
| 120 | 1848 | 1838 | 184661.58 | 185356.50 | -0.37 | 1817 | 1845 | 1837 |

Max Temp
Max Allowed

| Time (min) | Furnace Probe #4 (°F) | Furnace Probe #5 (°F) | Furnace Probe #6 (°F) | Furnace Probe #7 (°F) | Furnace Probe #8 (°F) | Furnace Probe #9 (°F) | Furnace Probe #10 (°F) | Furnace Probe #11 (°F) | Furnace Probe #12 (°F) |
|---------------|--------------------------------|--------------------------------|--------------------------------|--------------------------------|--------------------------------|--------------------------------|---------------------------------|---------------------------------|---------------------------------|
| 0 | 92 | 92 | 93 | 92 | 92 | 93 | 93 | 92 | 92 |
| 1 | 149 | 195 | 137 | 133 | 137 | 143 | 157 | 165 | 119 |
| 2 | 269 | 391 | 265 | 247 | 259 | 271 | 319 | 373 | 216 |
| 3 | 410 | 587 | 430 | 399 | 433 | 446 | 516 | 589 | 369 |
| 4 | 559 | 755 | 596 | 567 | 632 | 621 | 702 | 767 | 537 |
| 5 | 716 | 876 | 728 | 746 | 802 | 768 | 860 | 912 | 694 |
| 6 | 842 | 968 | 831 | 898 | 943 | 880 | 982 | 1017 | 824 |
| 7 | 950 | 1069 | 935 | 1028 | 1062 | 971 | 1064 | 1125 | 949 |
| 8 | 1055 | 1166 | 1037 | 1141 | 1169 | 1062 | 1141 | 1224 | 1071 |
| 9 | 1140 | 1242 | 1127 | 1225 | 1249 | 1138 | 1200 | 1293 | 1174 |
| 10 | 1206 | 1302 | 1198 | 1286 | 1311 | 1200 | 1245 | 1345 | 1256 |
| 11 | 1260 | 1352 | 1255 | 1333 | 1359 | 1250 | 1286 | 1389 | 1318 |
| 12 | 1307 | 1396 | 1306 | 1370 | 1399 | 1293 | 1318 | 1427 | 1369 |
| 13 | 1346 | 1434 | 1350 | 1404 | 1438 | 1329 | 1343 | 1458 | 1413 |
| 14 | 1376 | 1463 | 1385 | 1434 | 1468 | 1358 | 1362 | 1480 | 1448 |
| 15 | 1381 | 1459 | 1391 | 1434 | 1465 | 1356 | 1359 | 1464 | 1450 |
| 16 | 1392 | 1467 | 1403 | 1444 | 1473 | 1368 | 1370 | 1474 | 1462 |
| 17 | 1411 | 1481 | 1420 | 1459 | 1488 | 1383 | 1384 | 1490 | 1478 |
| 18 | 1427 | 1494 | 1436 | 1471 | 1500 | 1399 | 1398 | 1502 | 1492 |
| 19 | 1441 | 1505 | 1450 | 1482 | 1511 | 1410 | 1411 | 1512 | 1504 |
| 20 | 1454 | 1518 | 1464 | 1491 | 1524 | 1424 | 1425 | 1524 | 1517 |
| 21 | 1469 | 1531 | 1478 | 1505 | 1537 | 1439 | 1438 | 1536 | 1530 |
| 22 | 1479 | 1539 | 1489 | 1511 | 1546 | 1446 | 1451 | 1542 | 1539 |
| 23 | 1484 | 1541 | 1492 | 1514 | 1547 | 1446 | 1453 | 1540 | 1539 |
| 24 | 1492 | 1546 | 1497 | 1520 | 1552 | 1453 | 1462 | 1548 | 1542 |
| 25 | 1503 | 1557 | 1508 | 1530 | 1563 | 1465 | 1476 | 1562 | 1556 |
| 26 | 1516 | 1569 | 1522 | 1541 | 1576 | 1478 | 1491 | 1573 | 1568 |
| 27 | 1529 | 1580 | 1533 | 1554 | 1587 | 1490 | 1507 | 1585 | 1579 |
| 28 | 1540 | 1590 | 1543 | 1562 | 1598 | 1500 | 1522 | 1594 | 1589 |
| 29 | 1545 | 1592 | 1546 | 1566 | 1601 | 1498 | 1523 | 1595 | 1591 |
| 30 | 1548 | 1593 | 1547 | 1569 | 1602 | 1502 | 1535 | 1598 | 1592 |
| 31 | 1553 | 1599 | 1553 | 1573 | 1608 | 1510 | 1542 | 1605 | 1600 |
| 32 | 1561 | 1606 | 1561 | 1580 | 1615 | 1518 | 1557 | 1612 | 1607 |
| 33 | 1571 | 1614 | 1569 | 1590 | 1624 | 1529 | 1569 | 1620 | 1615 |
| 34 | 1580 | 1621 | 1576 | 1597 | 1631 | 1536 | 1582 | 1627 | 1623 |
| 35 | 1584 | 1624 | 1579 | 1600 | 1633 | 1539 | 1589 | 1628 | 1624 |
| 36 | 1589 | 1628 | 1582 | 1605 | 1637 | 1544 | 1600 | 1634 | 1627 |
| 37 | 1595 | 1634 | 1589 | 1611 | 1644 | 1552 | 1610 | 1641 | 1635 |
| 38 | 1605 | 1642 | 1598 | 1620 | 1653 | 1561 | 1622 | 1650 | 1643 |
| 39 | 1614 | 1651 | 1606 | 1628 | 1662 | 1571 | 1630 | 1659 | 1651 |
| 40 | 1623 | 1660 | 1614 | 1637 | 1670 | 1580 | 1643 | 1667 | 1658 |
| 41 | 1632 | 1668 | 1623 | 1645 | 1679 | 1590 | 1652 | 1673 | 1666 |
| 42 | 1640 | 1674 | 1629 | 1651 | 1685 | 1604 | 1663 | 1678 | 1671 |
| 43 | 1643 | 1676 | 1631 | 1653 | 1686 | 1609 | 1666 | 1677 | 1671 |
| 44 | 1638 | 1670 | 1626 | 1647 | 1680 | 1602 | 1657 | 1669 | 1665 |
| 45 | 1640 | 1670 | 1627 | 1648 | 1681 | 1607 | 1661 | 1669 | 1665 |
| 46 | 1645 | 1674 | 1629 | 1651 | 1683 | 1611 | 1666 | 1672 | 1669 |

| Time (min) | Furnace Probe #4 (°F) | Furnace Probe #5 (°F) | Furnace Probe #6 (°F) | Furnace Probe #7 (°F) | Furnace Probe #8 (°F) | Furnace Probe #9 (°F) | Furnace Probe #10 (°F) | Furnace Probe #11 (°F) | Furnace Probe #12 (°F) |
|---------------|--------------------------------|--------------------------------|--------------------------------|--------------------------------|--------------------------------|--------------------------------|---------------------------------|---------------------------------|---------------------------------|
| 47 | 1644 | 1673 | 1628 | 1651 | 1682 | 1608 | 1662 | 1669 | 1666 |
| 48 | 1650 | 1678 | 1634 | 1655 | 1688 | 1617 | 1672 | 1677 | 1671 |
| 49 | 1658 | 1686 | 1641 | 1662 | 1695 | 1626 | 1683 | 1684 | 1679 |
| 50 | 1665 | 1693 | 1647 | 1668 | 1703 | 1634 | 1693 | 1692 | 1685 |
| 51 | 1669 | 1696 | 1651 | 1672 | 1706 | 1637 | 1694 | 1694 | 1688 |
| 52 | 1677 | 1702 | 1658 | 1679 | 1712 | 1645 | 1704 | 1700 | 1694 |
| 53 | 1678 | 1702 | 1658 | 1680 | 1713 | 1650 | 1704 | 1700 | 1695 |
| 54 | 1680 | 1702 | 1659 | 1681 | 1713 | 1650 | 1707 | 1700 | 1695 |
| 55 | 1681 | 1703 | 1659 | 1682 | 1714 | 1652 | 1708 | 1701 | 1695 |
| 56 | 1677 | 1698 | 1654 | 1677 | 1707 | 1641 | 1694 | 1689 | 1687 |
| 57 | 1679 | 1700 | 1656 | 1678 | 1709 | 1651 | 1702 | 1697 | 1689 |
| 58 | 1690 | 1709 | 1664 | 1688 | 1719 | 1661 | 1716 | 1707 | 1699 |
| 59 | 1698 | 1717 | 1672 | 1696 | 1727 | 1671 | 1727 | 1716 | 1707 |
| 60 | 1705 | 1723 | 1678 | 1703 | 1735 | 1677 | 1735 | 1722 | 1715 |
| 61 | 1704 | 1722 | 1677 | 1702 | 1734 | 1676 | 1731 | 1719 | 1713 |
| 62 | 1709 | 1726 | 1682 | 1706 | 1738 | 1683 | 1739 | 1725 | 1717 |
| 63 | 1714 | 1731 | 1686 | 1710 | 1743 | 1686 | 1746 | 1729 | 1722 |
| 64 | 1716 | 1732 | 1688 | 1712 | 1745 | 1690 | 1746 | 1730 | 1724 |
| 65 | 1718 | 1735 | 1691 | 1714 | 1748 | 1695 | 1751 | 1733 | 1726 |
| 66 | 1721 | 1739 | 1696 | 1717 | 1754 | 1701 | 1755 | 1740 | 1730 |
| 67 | 1726 | 1744 | 1700 | 1722 | 1758 | 1703 | 1760 | 1744 | 1735 |
| 68 | 1730 | 1746 | 1704 | 1727 | 1762 | 1707 | 1765 | 1748 | 1739 |
| 69 | 1732 | 1747 | 1705 | 1728 | 1763 | 1711 | 1764 | 1747 | 1740 |
| 70 | 1736 | 1752 | 1709 | 1731 | 1768 | 1712 | 1770 | 1751 | 1744 |
| 71 | 1737 | 1754 | 1711 | 1733 | 1770 | 1713 | 1770 | 1753 | 1746 |
| 72 | 1742 | 1758 | 1715 | 1737 | 1775 | 1719 | 1775 | 1758 | 1750 |
| 73 | 1746 | 1761 | 1718 | 1741 | 1779 | 1721 | 1778 | 1760 | 1754 |
| 74 | 1743 | 1760 | 1717 | 1738 | 1778 | 1719 | 1773 | 1757 | 1752 |
| 75 | 1747 | 1765 | 1722 | 1743 | 1783 | 1723 | 1779 | 1763 | 1757 |
| 76 | 1749 | 1766 | 1724 | 1745 | 1785 | 1726 | 1780 | 1765 | 1758 |
| 77 | 1754 | 1770 | 1729 | 1749 | 1791 | 1731 | 1786 | 1770 | 1763 |
| 78 | 1757 | 1775 | 1734 | 1753 | 1796 | 1736 | 1790 | 1775 | 1769 |
| 79 | 1760 | 1779 | 1738 | 1756 | 1802 | 1741 | 1793 | 1780 | 1773 |
| 80 | 1758 | 1778 | 1736 | 1754 | 1799 | 1737 | 1787 | 1777 | 1771 |
| 81 | 1764 | 1782 | 1741 | 1759 | 1804 | 1740 | 1792 | 1782 | 1776 |
| 82 | 1763 | 1783 | 1741 | 1758 | 1804 | 1735 | 1788 | 1781 | 1775 |
| 83 | 1768 | 1788 | 1746 | 1764 | 1810 | 1743 | 1796 | 1786 | 1782 |
| 84 | 1772 | 1792 | 1750 | 1767 | 1815 | 1748 | 1800 | 1791 | 1786 |
| 85 | 1771 | 1791 | 1750 | 1766 | 1815 | 1747 | 1799 | 1789 | 1784 |
| 86 | 1775 | 1795 | 1754 | 1770 | 1820 | 1749 | 1805 | 1794 | 1789 |
| 87 | 1780 | 1799 | 1758 | 1775 | 1825 | 1756 | 1809 | 1798 | 1794 |
| 88 | 1781 | 1801 | 1761 | 1777 | 1827 | 1758 | 1810 | 1801 | 1797 |
| 89 | 1785 | 1804 | 1765 | 1780 | 1831 | 1759 | 1814 | 1804 | 1801 |
| 90 | 1788 | 1808 | 1768 | 1783 | 1836 | 1762 | 1817 | 1807 | 1805 |
| 91 | 1791 | 1812 | 1772 | 1786 | 1840 | 1763 | 1820 | 1810 | 1808 |
| 92 | 1794 | 1815 | 1775 | 1789 | 1844 | 1764 | 1822 | 1812 | 1811 |
| 93 | 1796 | 1817 | 1777 | 1790 | 1846 | 1765 | 1823 | 1813 | 1813 |

| Time (min) | Furnace Probe #4 (°F) | Furnace Probe #5 (°F) | Furnace Probe #6 (°F) | Furnace Probe #7 (°F) | Furnace Probe #8 (°F) | Furnace Probe #9 (°F) | Furnace Probe #10 (°F) | Furnace Probe #11 (°F) | Furnace Probe #12 (°F) |
|-----------------------|--|--|--|--|--|--|---|---|---|
| 94 | 1797 | 1817 | 1778 | 1791 | 1846 | 1763 | 1820 | 1814 | 1812 |
| 95 | 1796 | 1816 | 1776 | 1790 | 1844 | 1764 | 1819 | 1813 | 1811 |
| 96 | 1801 | 1821 | 1780 | 1795 | 1850 | 1768 | 1826 | 1819 | 1816 |
| 97 | 1804 | 1825 | 1784 | 1798 | 1854 | 1774 | 1831 | 1822 | 1820 |
| 98 | 1807 | 1826 | 1787 | 1801 | 1856 | 1774 | 1833 | 1823 | 1821 |
| 99 | 1802 | 1819 | 1782 | 1794 | 1850 | 1767 | 1823 | 1817 | 1816 |
| 100 | 1807 | 1824 | 1785 | 1798 | 1854 | 1771 | 1830 | 1822 | 1819 |
| 101 | 1810 | 1827 | 1788 | 1802 | 1858 | 1775 | 1834 | 1825 | 1823 |
| 102 | 1814 | 1832 | 1792 | 1806 | 1863 | 1778 | 1838 | 1828 | 1826 |
| 103 | 1817 | 1834 | 1793 | 1809 | 1866 | 1782 | 1841 | 1831 | 1828 |
| 104 | 1819 | 1836 | 1795 | 1810 | 1869 | 1782 | 1843 | 1835 | 1831 |
| 105 | 1819 | 1836 | 1797 | 1810 | 1870 | 1783 | 1842 | 1835 | 1832 |
| 106 | 1819 | 1838 | 1797 | 1810 | 1870 | 1783 | 1841 | 1835 | 1833 |
| 107 | 1818 | 1838 | 1796 | 1810 | 1869 | 1783 | 1840 | 1833 | 1831 |
| 108 | 1815 | 1833 | 1793 | 1806 | 1865 | 1778 | 1833 | 1828 | 1827 |
| 109 | 1818 | 1836 | 1797 | 1809 | 1869 | 1784 | 1839 | 1833 | 1831 |
| 110 | 1821 | 1837 | 1799 | 1811 | 1872 | 1787 | 1842 | 1836 | 1833 |
| 111 | 1823 | 1839 | 1802 | 1814 | 1875 | 1788 | 1845 | 1839 | 1836 |
| 112 | 1826 | 1842 | 1803 | 1816 | 1876 | 1791 | 1846 | 1841 | 1837 |
| 113 | 1830 | 1848 | 1806 | 1821 | 1879 | 1795 | 1851 | 1844 | 1841 |
| 114 | 1834 | 1855 | 1809 | 1825 | 1881 | 1798 | 1856 | 1848 | 1845 |
| 115 | 1835 | 1854 | 1811 | 1826 | 1884 | 1800 | 1857 | 1850 | 1847 |
| 116 | 1837 | 1854 | 1812 | 1827 | 1886 | 1803 | 1860 | 1851 | 1849 |
| 117 | 1840 | 1858 | 1814 | 1830 | 1888 | 1805 | 1862 | 1852 | 1850 |
| 118 | 1841 | 1858 | 1817 | 1832 | 1891 | 1807 | 1865 | 1855 | 1853 |
| 119 | 1832 | 1849 | 1809 | 1823 | 1881 | 1794 | 1849 | 1844 | 1842 |
| 120 | 1835 | 1852 | 1811 | 1825 | 1883 | 1802 | 1856 | 1849 | 1846 |

Max Temp
Max Allowed

| Time (min) | Cold Side Min (°F) | Cold Side Avg (°F) | Cold Side Max (°F) | Cold Side TC #1 (°F) | Cold Side TC #2 (°F) | Cold Side TC #3 (°F) | Cold Side TC #4 (°F) | Cold Side TC #5 (°F) | Cold Side TC #6 (°F) | Cold Side TC #7 (°F) | Cold Side TC #8 (°F) | Cold Side TC #9 (°F) | Lab Ambient (°F) | |
|---------------|-----------------------------|-----------------------------|-----------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|------------------------|----|
| 0 | 87 | 88 | 89 | 88 | 89 | 89 | 88 | 88 | 88 | 88 | 89 | 87 | 88 | |
| 1 | 87 | 88 | 89 | 88 | 89 | 89 | 88 | 88 | 88 | 87 | 89 | 87 | 88 | |
| 2 | 88 | 88 | 89 | 88 | 89 | 89 | 88 | 88 | 88 | 88 | 89 | 88 | 88 | |
| 3 | 88 | 88 | 89 | 88 | 89 | 89 | 88 | 88 | 89 | 88 | 89 | 88 | 89 | |
| 4 | 88 | 89 | 89 | 88 | 89 | 89 | 89 | 89 | 89 | 88 | 89 | 88 | 89 | |
| 5 | 88 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 88 | 89 | 88 | 89 |
| 6 | 88 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 88 | 89 | 88 | 90 |
| 7 | 88 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 88 | 89 | 88 | 90 |
| 8 | 88 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 88 | 89 | 88 | 89 |
| 9 | 88 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 88 | 89 | 88 | 89 |
| 10 | 88 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 88 | 89 | 88 | 91 |
| 11 | 88 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 88 | 89 | 88 | 91 |
| 12 | 88 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 88 | 89 | 88 | 91 |
| 13 | 88 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 88 | 89 | 88 | 91 |
| 14 | 88 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 88 | 89 | 88 | 91 |
| 15 | 88 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 88 | 89 | 88 | 90 |
| 16 | 88 | 89 | 90 | 89 | 90 | 89 | 89 | 89 | 89 | 89 | 88 | 89 | 88 | 89 |
| 17 | 88 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 88 | 89 | 88 | 90 |
| 18 | 88 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 88 | 89 | 88 | 89 |
| 19 | 88 | 89 | 90 | 89 | 90 | 89 | 89 | 89 | 89 | 89 | 88 | 89 | 88 | 90 |
| 20 | 88 | 89 | 90 | 89 | 90 | 89 | 89 | 89 | 89 | 89 | 88 | 89 | 88 | 90 |
| 21 | 88 | 89 | 90 | 89 | 90 | 89 | 89 | 89 | 89 | 89 | 88 | 89 | 88 | 90 |
| 22 | 88 | 89 | 90 | 89 | 90 | 90 | 89 | 89 | 89 | 89 | 88 | 90 | 89 | 90 |
| 23 | 88 | 89 | 90 | 90 | 90 | 90 | 89 | 89 | 89 | 89 | 88 | 90 | 89 | 90 |
| 24 | 89 | 90 | 91 | 91 | 90 | 90 | 89 | 89 | 89 | 89 | 89 | 90 | 89 | 90 |
| 25 | 89 | 90 | 93 | 93 | 91 | 90 | 89 | 89 | 90 | 89 | 90 | 90 | 89 | 91 |
| 26 | 89 | 90 | 95 | 95 | 91 | 90 | 90 | 90 | 90 | 90 | 89 | 90 | 89 | 89 |
| 27 | 89 | 91 | 98 | 98 | 92 | 90 | 90 | 90 | 90 | 90 | 89 | 90 | 89 | 91 |
| 28 | 89 | 91 | 101 | 101 | 93 | 90 | 90 | 90 | 90 | 90 | 89 | 90 | 89 | 91 |
| 29 | 89 | 92 | 104 | 104 | 94 | 90 | 90 | 90 | 91 | 89 | 90 | 90 | 89 | 90 |
| 30 | 89 | 93 | 107 | 107 | 96 | 91 | 90 | 90 | 92 | 89 | 90 | 90 | 89 | 91 |
| 31 | 89 | 93 | 110 | 110 | 98 | 91 | 90 | 90 | 93 | 89 | 91 | 91 | 89 | 91 |
| 32 | 89 | 94 | 113 | 113 | 99 | 91 | 90 | 90 | 95 | 89 | 91 | 91 | 90 | 91 |
| 33 | 89 | 95 | 115 | 115 | 101 | 91 | 90 | 90 | 97 | 89 | 91 | 91 | 90 | 91 |
| 34 | 89 | 96 | 118 | 118 | 102 | 92 | 90 | 90 | 98 | 89 | 91 | 91 | 90 | 91 |
| 35 | 89 | 96 | 120 | 120 | 104 | 92 | 90 | 90 | 100 | 89 | 91 | 91 | 90 | 92 |
| 36 | 89 | 97 | 122 | 122 | 105 | 92 | 90 | 90 | 102 | 89 | 91 | 91 | 90 | 91 |
| 37 | 89 | 98 | 124 | 124 | 107 | 93 | 91 | 90 | 104 | 89 | 91 | 91 | 90 | 92 |
| 38 | 90 | 99 | 126 | 126 | 109 | 94 | 91 | 91 | 105 | 90 | 91 | 91 | 90 | 92 |
| 39 | 90 | 99 | 128 | 128 | 110 | 94 | 91 | 91 | 107 | 90 | 92 | 92 | 90 | 93 |
| 40 | 90 | 100 | 130 | 130 | 112 | 95 | 92 | 91 | 109 | 90 | 92 | 92 | 90 | 94 |
| 41 | 90 | 101 | 132 | 132 | 113 | 96 | 92 | 91 | 110 | 90 | 92 | 92 | 90 | 93 |
| 42 | 91 | 102 | 134 | 134 | 115 | 98 | 93 | 91 | 112 | 91 | 92 | 92 | 91 | 93 |
| 43 | 91 | 103 | 135 | 135 | 116 | 99 | 94 | 92 | 113 | 91 | 92 | 92 | 91 | 93 |
| 44 | 91 | 104 | 137 | 137 | 118 | 100 | 96 | 92 | 114 | 92 | 92 | 92 | 91 | 93 |
| 45 | 91 | 105 | 139 | 139 | 119 | 102 | 97 | 93 | 116 | 92 | 92 | 92 | 91 | 94 |
| 46 | 91 | 105 | 140 | 140 | 121 | 103 | 98 | 93 | 117 | 93 | 92 | 92 | 91 | 94 |

| Time (min) | Cold Side Min (°F) | Cold Side Avg (°F) | Cold Side Max (°F) | Cold Side TC #1 (°F) | Cold Side TC #2 (°F) | Cold Side TC #3 (°F) | Cold Side TC #4 (°F) | Cold Side TC #5 (°F) | Cold Side TC #6 (°F) | Cold Side TC #7 (°F) | Cold Side TC #8 (°F) | Cold Side TC #9 (°F) | Lab Ambient (°F) |
|---------------|-----------------------------|-----------------------------|-----------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|------------------------|
| 47 | 91 | 107 | 142 | 142 | 123 | 105 | 100 | 94 | 118 | 94 | 93 | 91 | 95 |
| 48 | 92 | 108 | 144 | 144 | 124 | 107 | 102 | 95 | 120 | 95 | 93 | 92 | 94 |
| 49 | 92 | 109 | 145 | 145 | 125 | 109 | 103 | 96 | 121 | 96 | 93 | 92 | 95 |
| 50 | 92 | 110 | 146 | 146 | 126 | 111 | 105 | 97 | 122 | 97 | 93 | 92 | 92 |
| 51 | 92 | 111 | 148 | 148 | 128 | 113 | 107 | 98 | 123 | 97 | 94 | 92 | 93 |
| 52 | 92 | 112 | 149 | 149 | 129 | 115 | 108 | 99 | 124 | 98 | 96 | 92 | 93 |
| 53 | 93 | 114 | 150 | 150 | 130 | 116 | 110 | 100 | 126 | 99 | 98 | 93 | 93 |
| 54 | 93 | 115 | 151 | 151 | 131 | 118 | 111 | 102 | 127 | 100 | 99 | 93 | 93 |
| 55 | 93 | 116 | 152 | 152 | 133 | 120 | 113 | 103 | 128 | 100 | 101 | 93 | 93 |
| 56 | 94 | 117 | 153 | 153 | 134 | 122 | 114 | 104 | 129 | 101 | 103 | 94 | 92 |
| 57 | 94 | 118 | 154 | 154 | 135 | 124 | 116 | 105 | 130 | 102 | 105 | 94 | 93 |
| 58 | 94 | 119 | 155 | 155 | 136 | 126 | 117 | 106 | 131 | 103 | 107 | 94 | 93 |
| 59 | 95 | 121 | 156 | 156 | 137 | 128 | 119 | 107 | 132 | 104 | 110 | 95 | 91 |
| 60 | 96 | 122 | 157 | 157 | 138 | 129 | 120 | 108 | 133 | 105 | 112 | 96 | 93 |
| 61 | 96 | 123 | 158 | 158 | 139 | 131 | 122 | 109 | 134 | 106 | 113 | 96 | 93 |
| 62 | 97 | 124 | 159 | 159 | 140 | 133 | 123 | 110 | 135 | 107 | 115 | 97 | 94 |
| 63 | 97 | 125 | 159 | 159 | 142 | 134 | 125 | 112 | 136 | 107 | 117 | 97 | 93 |
| 64 | 98 | 127 | 160 | 160 | 142 | 136 | 126 | 113 | 137 | 108 | 119 | 98 | 93 |
| 65 | 98 | 128 | 161 | 161 | 143 | 137 | 128 | 114 | 138 | 109 | 121 | 98 | 94 |
| 66 | 99 | 129 | 161 | 161 | 144 | 139 | 129 | 115 | 138 | 110 | 122 | 99 | 93 |
| 67 | 99 | 130 | 162 | 162 | 146 | 140 | 130 | 116 | 139 | 111 | 124 | 99 | 93 |
| 68 | 99 | 130 | 162 | 162 | 146 | 142 | 131 | 117 | 140 | 112 | 125 | 99 | 94 |
| 69 | 100 | 132 | 163 | 163 | 147 | 143 | 133 | 118 | 141 | 113 | 126 | 100 | 94 |
| 70 | 101 | 132 | 163 | 163 | 146 | 144 | 134 | 119 | 141 | 113 | 128 | 101 | 94 |
| 71 | 101 | 133 | 163 | 163 | 148 | 145 | 135 | 120 | 142 | 115 | 129 | 101 | 94 |
| 72 | 101 | 134 | 164 | 164 | 149 | 146 | 136 | 121 | 143 | 116 | 130 | 101 | 95 |
| 73 | 102 | 135 | 164 | 164 | 149 | 147 | 137 | 122 | 143 | 117 | 131 | 102 | 94 |
| 74 | 102 | 135 | 164 | 164 | 150 | 148 | 138 | 123 | 144 | 118 | 132 | 102 | 93 |
| 75 | 103 | 137 | 165 | 165 | 151 | 149 | 139 | 124 | 145 | 119 | 134 | 103 | 93 |
| 76 | 103 | 137 | 165 | 165 | 151 | 150 | 140 | 125 | 145 | 120 | 135 | 103 | 93 |
| 77 | 103 | 138 | 165 | 165 | 152 | 151 | 141 | 126 | 146 | 121 | 135 | 103 | 92 |
| 78 | 103 | 138 | 165 | 165 | 152 | 151 | 142 | 127 | 147 | 122 | 137 | 103 | 92 |
| 79 | 104 | 139 | 165 | 165 | 152 | 152 | 142 | 128 | 147 | 123 | 137 | 104 | 91 |
| 80 | 104 | 139 | 165 | 165 | 152 | 153 | 143 | 129 | 147 | 124 | 138 | 104 | 93 |
| 81 | 105 | 140 | 165 | 165 | 153 | 153 | 144 | 130 | 148 | 125 | 139 | 105 | 93 |
| 82 | 105 | 141 | 165 | 165 | 154 | 154 | 145 | 131 | 149 | 126 | 140 | 105 | 92 |
| 83 | 105 | 142 | 166 | 166 | 154 | 155 | 146 | 132 | 149 | 127 | 141 | 105 | 93 |
| 84 | 106 | 142 | 166 | 166 | 154 | 155 | 147 | 132 | 150 | 128 | 141 | 106 | 94 |
| 85 | 106 | 143 | 166 | 166 | 154 | 156 | 147 | 134 | 150 | 129 | 142 | 106 | 94 |
| 86 | 107 | 143 | 166 | 166 | 155 | 156 | 148 | 134 | 151 | 130 | 143 | 107 | 94 |
| 87 | 107 | 144 | 166 | 166 | 156 | 157 | 149 | 135 | 151 | 131 | 144 | 107 | 94 |
| 88 | 107 | 144 | 166 | 166 | 156 | 157 | 149 | 136 | 152 | 132 | 145 | 107 | 95 |
| 89 | 108 | 145 | 166 | 166 | 156 | 158 | 150 | 137 | 152 | 133 | 145 | 108 | 95 |
| 90 | 108 | 145 | 166 | 166 | 156 | 158 | 151 | 137 | 152 | 134 | 146 | 108 | 94 |
| 91 | 109 | 146 | 166 | 166 | 157 | 159 | 151 | 138 | 153 | 135 | 147 | 109 | 95 |
| 92 | 109 | 147 | 166 | 166 | 158 | 159 | 152 | 139 | 153 | 136 | 147 | 109 | 95 |
| 93 | 109 | 147 | 166 | 166 | 157 | 159 | 152 | 140 | 153 | 137 | 148 | 109 | 95 |

| Time (min) | Cold Side Min (°F) | Cold Side Avg (°F) | Cold Side Max (°F) | Cold Side TC #1 (°F) | Cold Side TC #2 (°F) | Cold Side TC #3 (°F) | Cold Side TC #4 (°F) | Cold Side TC #5 (°F) | Cold Side TC #6 (°F) | Cold Side TC #7 (°F) | Cold Side TC #8 (°F) | Cold Side TC #9 (°F) | Lab Ambient (°F) |
|--------------------|-----------------------------|-----------------------------|-----------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|------------------------|
| 94 | 110 | 147 | 166 | 166 | 158 | 160 | 153 | 140 | 154 | 138 | 148 | 110 | 95 |
| 95 | 110 | 148 | 166 | 166 | 158 | 160 | 153 | 141 | 154 | 138 | 149 | 110 | 95 |
| 96 | 111 | 148 | 166 | 166 | 158 | 160 | 154 | 142 | 155 | 140 | 149 | 111 | 95 |
| 97 | 111 | 149 | 166 | 166 | 158 | 161 | 154 | 142 | 155 | 140 | 150 | 111 | 96 |
| 98 | 112 | 149 | 166 | 166 | 158 | 161 | 154 | 143 | 155 | 141 | 150 | 112 | 94 |
| 99 | 112 | 149 | 166 | 166 | 159 | 161 | 155 | 143 | 156 | 142 | 151 | 112 | 96 |
| 100 | 113 | 150 | 166 | 166 | 159 | 162 | 155 | 144 | 156 | 143 | 151 | 113 | 96 |
| 101 | 113 | 150 | 166 | 166 | 159 | 162 | 155 | 144 | 156 | 143 | 151 | 113 | 94 |
| 102 | 114 | 150 | 166 | 166 | 159 | 162 | 156 | 145 | 156 | 144 | 152 | 114 | 95 |
| 103 | 115 | 151 | 166 | 166 | 159 | 162 | 156 | 145 | 155 | 145 | 152 | 115 | 96 |
| 104 | 115 | 151 | 166 | 166 | 158 | 162 | 156 | 146 | 155 | 146 | 153 | 115 | 97 |
| 105 | 116 | 151 | 165 | 165 | 160 | 162 | 156 | 146 | 155 | 146 | 153 | 116 | 97 |
| 106 | 116 | 151 | 165 | 165 | 159 | 163 | 157 | 147 | 155 | 147 | 153 | 116 | 96 |
| 107 | 117 | 152 | 165 | 165 | 159 | 163 | 157 | 147 | 156 | 147 | 154 | 117 | 97 |
| 108 | 117 | 152 | 165 | 165 | 160 | 163 | 157 | 148 | 156 | 148 | 154 | 117 | 96 |
| 109 | 118 | 152 | 165 | 165 | 160 | 163 | 157 | 148 | 156 | 148 | 154 | 118 | 95 |
| 110 | 119 | 152 | 165 | 165 | 158 | 163 | 157 | 148 | 155 | 149 | 154 | 119 | 96 |
| 111 | 119 | 153 | 165 | 165 | 159 | 163 | 157 | 149 | 156 | 150 | 155 | 119 | 96 |
| 112 | 120 | 153 | 165 | 165 | 160 | 163 | 157 | 149 | 156 | 150 | 155 | 120 | 95 |
| 113 | 120 | 153 | 165 | 165 | 159 | 163 | 158 | 149 | 156 | 150 | 155 | 120 | 94 |
| 114 | 121 | 153 | 165 | 165 | 160 | 163 | 158 | 150 | 156 | 151 | 155 | 121 | 96 |
| 115 | 122 | 154 | 165 | 165 | 159 | 164 | 158 | 150 | 157 | 152 | 156 | 122 | 96 |
| 116 | 122 | 154 | 165 | 165 | 160 | 164 | 158 | 150 | 157 | 152 | 156 | 122 | 97 |
| 117 | 123 | 154 | 165 | 165 | 160 | 164 | 158 | 150 | 157 | 152 | 156 | 123 | 96 |
| 118 | 123 | 154 | 165 | 165 | 161 | 164 | 158 | 151 | 157 | 153 | 156 | 123 | 96 |
| 119 | 124 | 154 | 165 | 165 | 160 | 164 | 159 | 151 | 157 | 153 | 156 | 124 | 97 |
| 120 | 125 | 154 | 164 | 164 | 160 | 164 | 159 | 151 | 157 | 153 | 156 | 125 | 97 |
| Max Temp | 125 | 154 | 166 | 166 | 161 | 164 | 159 | 151 | 157 | 153 | 156 | 125 | |
| Max Allowed | 412 | 338 | 414 | 413 | 414 | 414 | 413 | 413 | 413 | 413 | 414 | 412 | |

APPENDIX D

PHOTOGRAPHS







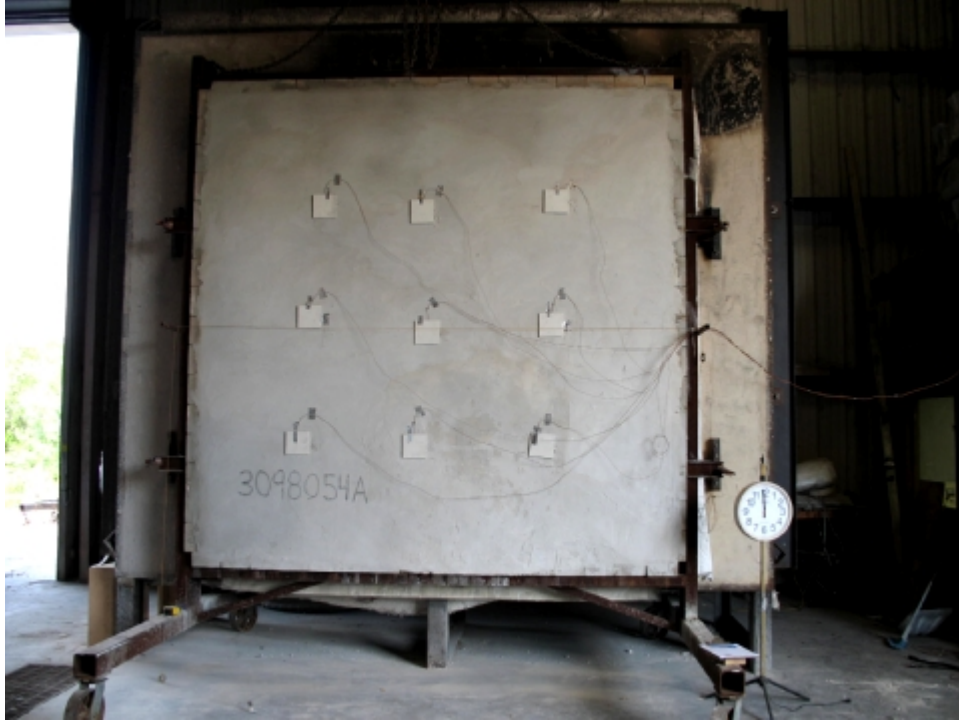


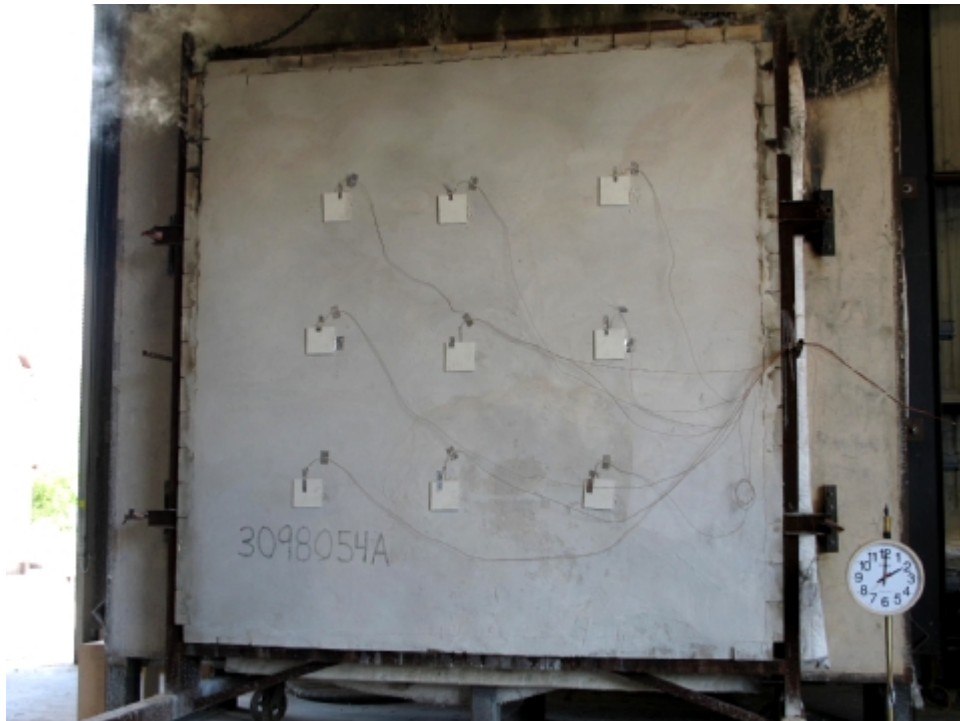




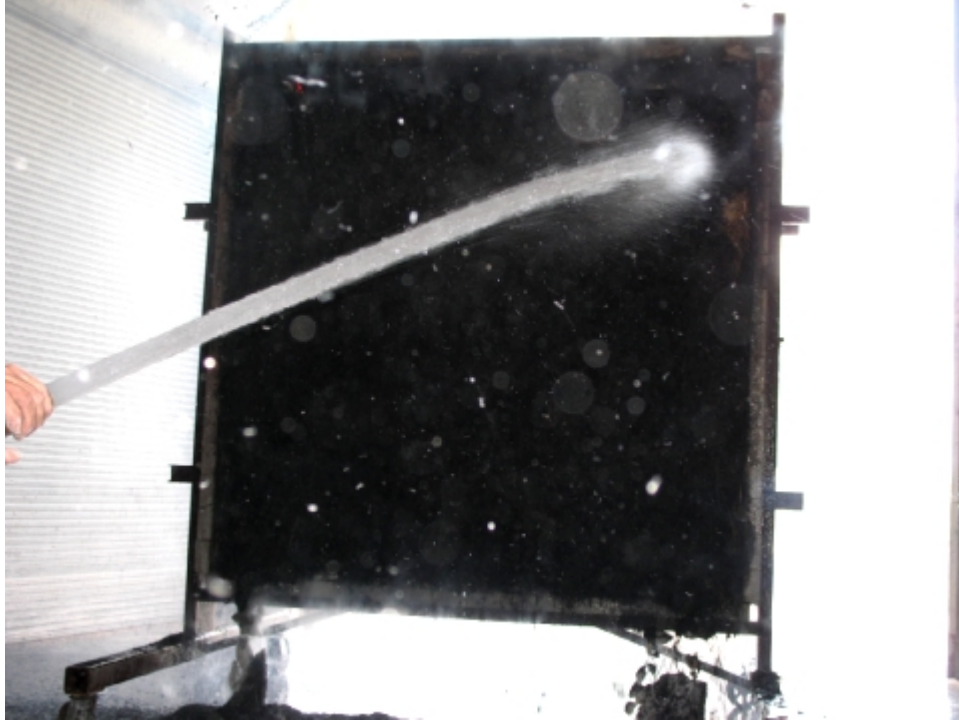


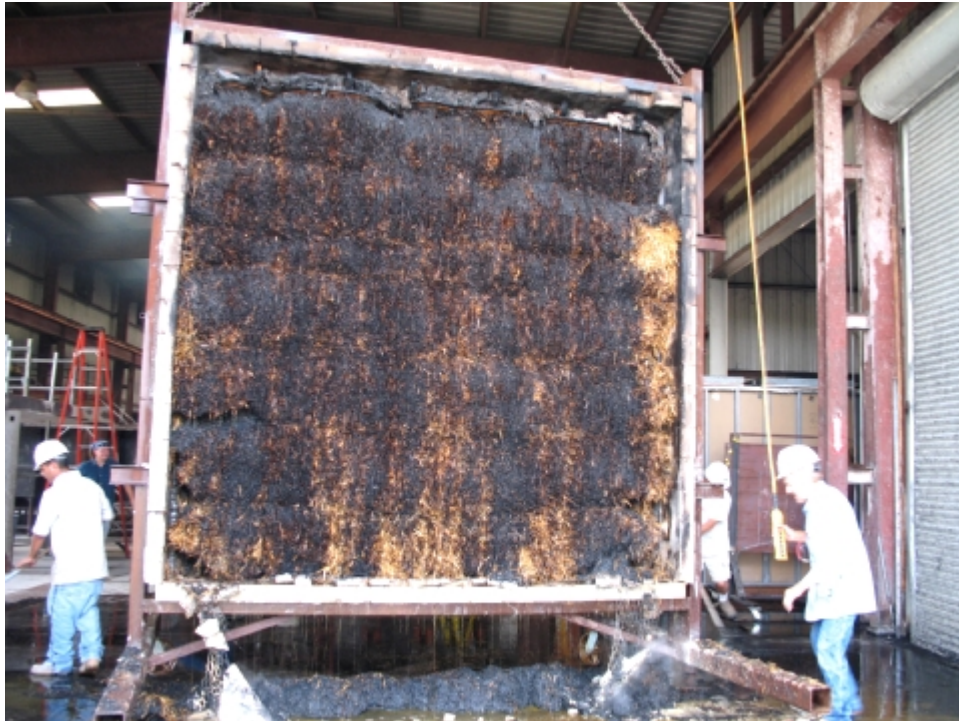












APPENDIX E

ASTM C 42 COMPRESSION RESULTS

LABORATORY TESTING REPORT



Raba Kistner Consultants, Inc.
 12821 W. Golden Lane
 P.O. Box 690287, San Antonio, TX 78269-0287
 (210) 699-9090 • FAX (210) 699-6426
 www.rkci.com

CLIENT: Intertek Testing
 16015 Shady Falls Road
 Elmendorf, Texas 78112-9784
 Attn: Mr. Mike Dey

PROJECT NO.: ASD05-173-00
DATE RECEIVED: 06-30-06
SAMPLED BY: Client
DATE TESTED: 07-20-06
TESTED BY: C. Berger (R-K)
DATE REPORTED: 07-24-06

PROJECT: Testing Services (Intertek)

RE: Compressive Strength – Earthen Plaster & Straw Bale Clay

| Earthen Plaster (Cast 06-22-06): | | | |
|----------------------------------|---------------|-------------|----------------------------|
| Specimen No. | Area (sq.in.) | Load (lbs.) | Compressive Strength (psi) |
| 1 | 36.04 | 10,940 | 300 |
| 2 | 36.12 | 10,260 | 280 |
| Average (28 days): | | | 290 |

| Straw Bale Clay (Cast 06-05-06): | | | |
|----------------------------------|---------------|-------------|----------------------------|
| Specimen No. | Area (sq.in.) | Load (lbs.) | Compressive Strength (psi) |
| 1 | 36.07 | 7,780 | 220 |
| 2 | 36.22 | 8,290 | 230 |
| Average (45 days): | | | 225 |

NOTICE: Raba-Kistner Consultants, Inc. considers the data and information contained in this report to be proprietary. This information is intended only for the use of the recipient(s) named herein. Test results presented herein relate only to those items tested. This document and any information contained herein shall not be disclosed and shall not be duplicated or used in whole or in part for any purpose other than to evaluate test results without written approval from Raba-Kistner Consultants, Inc.

COPIES TO: Above (1)

RABA-KISTNER CONSULTANTS, INC.

BY: *K.W. Marquardt* 7/28/06



ASSIGNMENT NO.: S06-038017
 /dgp 07-25-06



Raba Kistner Consultants, Inc.
 12821 W. Golden Lane
 P.O. Box 690287, San Antonio, TX 78269-0287
 (210) 699-9090 • FAX (210) 699-8426
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CLIENT: Intertek Testing
 16015 Shady Falls Road
 Elmendorf, Texas 78112-9784
 Attn: Mr. Mike Dey

REPORT OF TESTS ON STUCCO CORES

| Project Name: Testing Services (Intertek) | | Date Cored: 07-19-06 | | Project No.: ASD05-173-00 | | Date Tested: 07-20-06 | | Assignment No.: S06-038017 | | |
|---|---------------------------|---------------------------|------------------|-----------------------------------|--------|-----------------------|------------------------------------|----------------------------|-------------------|--------------------------------------|
| Date Placed: Not Provided | | Average Area: 6.50 sq.in. | | Nominal Diameter, D: 2.877 inches | | | | | | |
| Age of Concrete: Not Provided | | | | | | | | | | |
| Core No. | Core Location | Unit Weight (pcf) | Length, L (inch) | | | Length Diameter L/D | Load (lbs.) | Compressive Strength (psi) | Correction Factor | Corrected Compressive Strength (psi) |
| | | | Cored | Sawed | Capped | | | | | |
| 1 | Straw Stucco Scratch Coat | 125.2 | 5.597 | 5.554 | 5.779 | 2.01 | 27,940 | 4,300 | 1.0 | 4,300 |
| 2 | Straw Stucco Scratch Coat | 133.7 | 5.652 | 5.512 | 5.766 | 2.00 | 29,930 | 4,600 | 1.0 | 4,600 |
| 1 | Cement Stucco | 112.6 | 4.381 | 4.246 | 4.479 | 1.56 | 10,040 | 1,540 | .9648 | 1,490 |
| 2 | Cement Stucco | 112.1 | 4.341 | 4.232 | 4.474 | 1.56 | 10,810 | 1,660 | .9648 | 1,600 |
| | | | | | | | Straw Stucco Scratch Coat Average: | | | 4,450 |
| | | | | | | | Cement Stucco: | | | 1,550 |

Remarks:

- (1) The compressive strength testing of these cores was conducted in accordance with ASTM C 42 procedures and per client's instructions.
- (2) The test cores were loaded perpendicular to the horizontal plane of concrete placement.
- (3) The test cores were dry at the time of testing.
- (4) The nominal maximum aggregate size: Not Applicable
- (5) The test samples were free of reinforcing steel.
- (6) The test cores were capped with a sulfur compound.
- (7) Cored by C. Berger at R-K on 07-19-06.

Prepared By: CB

Tested By: TW/CB

Copies To: Above (1)

RABA-KISTNER CONSULTANTS, INC.

By: *K.W. Margardt*

/ldgp 07-25-06

7/27/06

